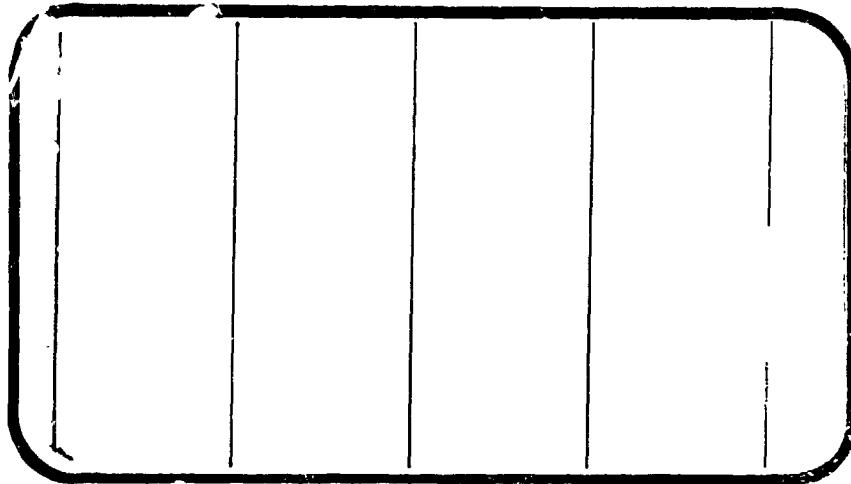


NASA

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NASA CR.

141513



(NASA-CR-141513) RESULTS OF INVESTIGATION
ON AN 0.004-SCALE 140C MODIFIED
CONFIGURATION SPACE SHUTTLE VEHICLE ORBITER
MODEL (74-0) IN THE NASA/LANGLEY RESEARCH
CENTER HYPERSONIC NITROGEN TUNNEL (OA89)

N75-21344

G3/18 Unclassified
 19244

SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT

JOHNSON SPACE CENTER
HOUSTON, TEXAS

DATA MANAGEMENT SERVICES
SPACE DIVISION CHRYSLER
CORPORATION

March, 1975

DMS-DR-2214
NASA CR-141,513

RESULTS OF INVESTIGATIONS ON AN 0.004-SCALE
140C MODIFIED CONFIGURATION SPACE SHUTTLE VEHICLE
ORBITER MODEL (74-0)
IN THE NASA/LANGLEY RESEARCH CENTER
HYPERSONIC NITROGEN TUNNEL (UA89)

By

P. J. Hawthorne
Shuttle Aero Sciences
Rockwell International Space Division

Prepared under NASA Contract Number: NAS9-13247

By

Data Management Services
Chrysler Corporation Space Division
New Orleans, La. 70189

for

Engineering Analysis Division

Johnson Space Center
National Aeronautics and Space Administration
Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Number: HNT 30, 31
NASA Series Number: OA29
Model Number: 74-0
Test Dates: 12 July through 6 August 1974 and
30 August through 5 September 1974
Occupancy Hours: 136

FACILITY COORDINATOR:

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Chrysler Corporation Space Division assumes no responsibility for the data presented other than display characteristics.

RESULTS OF INVESTIGATIONS ON AN 0.004-SCALE
140C MODIFIED CONFIGURATION SPACE SHUTTLE VEHICLE
ORBITER MODEL (74-0)
IN THE NASA/LANGLEY RESEARCH CENTER
HYPERSONIC NITROGEN TUNNEL (OA89)

By

P. J. Hawthorne, Rockwell International Space Division

ABSTRACT

This report documents data obtained during a wind tunnel test of an 0.004-scale 140C modified configuration SSV Orbiter in the NASA/Langley Research Center 22-inch Hypersonic Nitrogen Tunnel. The test was conducted during July, August and September 1974 and 136 occupancy hours were charged. All presented runs were conducted at a nominal Mach number of 19.8 and at a Reynolds number of approximately 0.68×10^6 per foot.

The complete 140C modified model was tested with various elevon settings and additionally in wing off/bodyflap off configuration at angles of attack from -5 to 42.5 degrees at zero yaw.

Purpose of this test was to obtain high hypersonic longitudinal and lateral-directional stability and control characteristics of the updated SSV configuration in an initially diatomic medium.

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* PLOT SCHEDULE:

- A) CN vs. ALPHA, CN vs. CLM, CL vs. ALPHA, CL vs. CLM, CA, CLM, L/D, and CD vs. ALPHA
- B) CY and CYN vs. ALPHA

NOMENCLATURE
General

<u>SIMBOL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
a		speed of sound; m/sec, ft/sec
C_p	CP	pressure coefficient; $(p_1 - p_\infty)/q$
M	MACH	Mach number; V/a
p		pressure; N/m ² , psf
q	$Q(\text{NSM})$ $Q(\text{PSF})$	dynamic pressure; $1/2 \rho V^2$, N/m ² , psf
RN/L	RN/L,RN	Reynolds number; based on model length
v		velocity; m/sec, ft/sec
α	ALPHA	angle of attack, degrees
β	BETA	angle of sideslip, degrees
ψ	PSI	angle of yaw, degrees
ϕ	PHI	angle of roll, degrees
ρ		mass density; kg/m ³ , slugs/ft ³

Reference & C.G. Definitions

A _b		base area; m ² , ft ²
b	E _{REF}	wing span or reference span; m, ft
c.g.		center of gravity
L_{REF}	L _{REF}	reference length or wing mean aerodynamic chord; m, ft
S	S _{REF}	wing area or reference area; m ² , ft ²
	MRP	moment reference point
	XMRP	moment reference point on X axis
	YMRP	moment reference point on Y axis
	ZMRP	moment reference point on Z axis

SUBSCRIPTS

b	base
l	local
s	static conditions
t	total conditions
∞	free stream

NOMENCLATURE (Continued)

Body-Axis System

<u>SIMBOL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
C_N	CN	normal-force coefficient; $\frac{\text{normal force}}{qS}$
C_A	CA	axial-force coefficient; $\frac{\text{axial force}}{qS}$
C_Y	CY	side-force coefficient; $\frac{\text{side force}}{qS}$
C_{A_b}	CAB	base-force coefficient; $\frac{\text{base force}}{qS}$ $-A_b(p_b - p_\infty)/qS$
C_{A_f}	CAF	forebody axial force coefficient, $C_A - C_{A_b}$
C_m	CIM	pitching-moment coefficient; $\frac{\text{pitching moment}}{qS_{\text{REF}}}$
C_n	CYN	yawing-moment coefficient; $\frac{\text{yawing moment}}{qS_b}$
C_l	CEL	rolling-moment coefficient; $\frac{\text{rolling moment}}{qS_b}$

Stability-Axis System

C_L	CL	lift coefficient; $\frac{\text{lift}}{qS}$
C_D	CD	drag coefficient; $\frac{\text{drag}}{qS}$
C_{D_b}	CDB	base-drag coefficient; $\frac{\text{base drag}}{qS}$
C_{D_f}	CDF	forebody drag coefficient; $C_D - C_{D_b}$
C_Y	CY	side-force coefficient; $\frac{\text{side force}}{qS}$
C_m	CIM	pitching-moment coefficient; $\frac{\text{pitching moment}}{qS_{\text{REF}}}$
C_n	CLN	yawing-moment coefficient; $\frac{\text{yawing moment}}{qS_b}$
C_l	CSL	rolling-moment coefficient; $\frac{\text{rolling moment}}{qS_b}$
L/D	L'/D	lift-to-drag ratio; C_L/C_D
L/D_f	L/DF	lift to forebody drag ratio; C_L/C_{D_f}

NOMENCLATURE (Continued)
Additional Nomenclature

<u>Symbol</u>	<u>Plot Symbol</u>	<u>Definition</u>
IML		inner mold line
MRC		moment reference center
OML		outer mold line
X_{cp}/ℓ_B	XCP/L	longitudinal center of pressure location, fraction of body length
X_0		Orbiter longitudinal station, in.
Y_0		Orbiter lateral station, in
Z_0		Orbiter vertical station, in
α_i		wing incidence angle, degrees
δ_{BF}	BDFLAP	bodyflap deflection angle, degrees
δ_R	RUDDER	rudder deflection angle, degrees
δ_{SB}	SPDBRK	speedbrake deflection angle, degrees
δ_a	AILRON	aileron, total aileron deflection angle, degrees, (left aileron - right aileron)/2
δ_e	ELEVTR	elevator surface deflection angle, positive deflection trailing edge down, degrees
BALANC		parameter name to document balance utilized in testing, BALANC = 1 (LaRC HN05), BALANC = 2 (LaRC HN06), see Remarks section
STING		parameter name for sting, sting parameter values of 25 and 45 denote a 25° and 45° sting used for testing, respectively

REMARKS

OA89 was conducted in three distinct portions, from July 12 through July 29, July 30 to August 6 and from August 30 through September 5, 1974.

During the first time period, the model was installed in the tunnel on the Langley Research Center HNO 6 component water cooled balance on a 45° bent sting. On July 24 it was found that the model was running slightly yawed, and this along with certain balance problems prompted re-running of the basic configuration flows to determine incremental effects of these problems. On July 29, the thermocouple indicating balance water temperature indicated 32°F during the afternoon run, and subsequent investigation revealed a broken bellows in the water cooling line, and that ice had been forming in the balance due to evaporative cooling. A balance change was then made to the lower range HNO 5 component water cooled balance, still on the 45° bent sting.

From July 30 to August 6 selected runs were made with the HNO 5 instrument, and it was undertaken to rerun the test with an abbreviated run schedule due to time constraints on the 74-0 model utilization. The test article was then removed from the test section for use elsewhere; this entire entry is referred to by Langley Research Center as test HNT 30.

The second installation was made at the end of August to investigate suspected sting effects; this time the HNO 5 balance was used with a 25° bent sting. This is known as the HNT 31 test series. Base pressure data were taken with only one pressure tap during OA89, instead of the two shown in the pretest report. Data were collected at total pressures of 2200 and

REMARKS (Concluded)

5000 psi during both HNT 30 and HNT 31, but the $P_T = 2200$ psi data is considered to be of questionable quality and only the $P_T = 5000$ psi data utilizing the HNO 5 balance is presented here, and none of the HNO 6 balance data are presented.

CONFIGURATIONS INVESTIGATED

During test OA89, the 140C modified vehicle was tested in full up and wing off configurations. The basic aircraft is of blended wing body design with a double delta wing, full span elevons and a single centerline vertical tail with rudder and/or speedbrake capability. A bodyflap and short pod orbital maneuvering system (OMS) were mounted on the aft fuselage bottom edge and upper sidewalls, respectively.

The following letter designations are used to denote the components of the -140C modified configurations:

- B₆₂ Fuselage to the outer mold line contours of drawings VL70-000202B, -000200B & 000203 for the aft body contour (except OMS), the VL70-000202B drawing was used in lieu of the C revision specified on the VL70-000140C control drawing since the C revision was not available. The MPS nozzles are not simulated.
- C₁₂ Canopy to VL70-000202B lines; see B₆₂ above.
- E₄₃ Elevon used with VL70-000200B wing, with 6" gaps. The hinge-line is unswept and located at $X_0 = 1387$.
- F₁₀ Center pivot bodyflap hinge line at $X_0 = 1532$ and planform as denoted on VL70-000200B drawing.
- M₁₄ Baseline short nose Orbital Maneuvering System (OMS) pods mounted on the upper base of the fuselage. Shape is defined by drawing VL70-08457. Rocket engine nozzles are simulated.
- R₅ Rudder utilized with V₈ vertical tail and shown on VL70-000146A.
- V₈ 45° sweep leading edge single centerline mounted vertical tail of modified diamond section as per VL70-000146A.
- W₁₂₇ VL70-000200B wing. Wing is of 81°/45° sweep leading edge and is 6 inches F.S. thicker at the body than -140A. Airfoil is RIC modified NASA 0011.3 at $Y_0 = 199$, 0012-64 at theoretical tip. $\alpha_i = +0^\circ$ 30' dihedral = 3° 30' at TE., tip is defined by VL70-006092.

CONFIGURATIONS INVESTIGATED (Concluded)

Component descriptor sheets are given in Table III.

The tested configurations were denoted as:

140C modified = B₆₂ C₁₂ E₄₃ F₁₀ M₁₄ R₅ V₈ W₁₂₇

140C modified wing and body flap off = B₆₂ C₁₂ M₁₄ R₅ "

TEST FACILITY DESCRIPTION

The NASA/Langley Research Center 18-inch Hypersonic Nitrogen Tunnel is a blow down facility with a normal operational time of up to two hours for force and moment testing. This long run time is possible because the nitrogen is obtained in liquid form, mechanically pumped to 17,000 psig P_T , and then vaporized and heated to 2900°F T_T prior to entry into the nozzle. The test section is of the open jet variety with a water cooled diffusor that exits into a 60-foot diameter vacuum sphere.

Models are sting mounted on an injectable blade strut with externally controllable pitch capability and manually setable yaw freedom. Force testing is done utilizing 5 component water cooled internal strain gauge balances, with injection time kept to a absolute minimum (less than 5 seconds) to alleviate balance drift problems due to aerodynamic heating. Air is also blown on the model to cool it while in the retracted position between injections.

Recent calibrations of the tunnel indicate that the most satisfactory conditions to obtain force data are:

Total pressure = 5000 psi

Total temp = 3360°R

RN/foot = 0.68×10^6

Mach = 19.80

The most recent operational parameters of the contoured nozzle are best obtained from the LaRC Hypersonic Analysis Section (Phone (804) 827-2483).

TEST FACILITY DESCRIPTION (Concluded)

The tunnel is also equipped with an electron beam flow visualization device which allows color photographs with depth of field to be made of the flow system, allowing interpretation of shock interactions and flow separation phenomena.

DATA REDUCTION

Those data presented were obtained with the LaRC HNO 5 internal strain gauge balance at one set of tunnel conditions only (refer to the Remarks section). Data were converted to standard NASA force and moment coefficients and are presented about a nominal moment reference center in both stability and body axis systems.

Additionally, the normal force center of pressure is presented as:

$$X_{CP}/\ell_B = \frac{X_{CG}}{\ell_S} - \frac{C_m(\bar{c})}{CN} \frac{\ell_B}{\ell_B}$$

where X_{CP} is the longitudinal distance from the inner mold line nose station ($X_0 = 238$ inches full scale) to the center of pressure. X_{CG} is the distance from inner mold line to the moment reference point ($X_{CG} = X_{MRP} - 238 = 838.7$ inches). The body length (ℓ_B) is 1290.3 inches.

The following reference dimensions were used to reduce the data to coefficient form:

$$S_{ref} = 2690.0 \text{ ft}^2$$

$$L_{REF} = \bar{c} = 474.81 \text{ in.}$$

$$B_{REF} = b = 936.68 \text{ in.}$$

$$X_{MRP} = 1076.7 \text{ in. } X_0$$

$$Y_{MRP} = 0.0 \text{ in. } Y_0$$

$$Z_{MRP} = 375.0 \text{ in. } Z_0$$

TABLE I.

TEST : OA89

DATE : Jan., 1975

TEST CONDITIONS

BALANCE UTILIZED: HNO 5

	CAPACITY:	ACCURACY:	COEFFICIENT TOLERANCE:
NF	51 lbf	0.5%	
SF	3 lbf	0.5%	
AF	31 lbf	0.5%	
PM	5 in 1bf	0.5%	
RM	no flexure		
YM	3 in 1bf	0.5%	

COMMENTS: P_T 5000 psi

TABLE II.
TEST : LaRC M19NT 30;31 (ΦA89)
DATA SET/RUN NUMBER COLLATION SUMMARY

TEST RUN NUMBERS									
DATA SET IDENTIFIER	CONFIGURATION	SCHED.			PARAMETERS/VALUES		NO. OF RUNS	MACH NUMBERS (OR ALTERNATE INDEPENDENT VARIABLE)	
		α	β	S_2	$S_{2\alpha}$	$S_{2\beta}$		$S_{2\alpha\beta}$	$S_{2\beta\alpha}$
RQDCC	140C QRB 74°	A	0	0	0	0	55	-	-
		T	T	20	T	16.3	-	-	-
1									
2									
3									
4									
5	WINGS & BODY FLAF OF:			-	-	-			
6	140C QRB 74°	C	0	0	0	0	-	32	4
7		T	T	10	T	16.3	-	-	-
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TABLE III MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - B₄

GENERAL DESCRIPTION : Configuration 140C orbiter fuselage MCR 200-R₄.

Similar to 140A 'B fuselage except aft body revised and improved

midbody-wing-boot fairing X₀ = 950 to X₀ = 1040.

MODEL SCALE: 0.004

DRAWING NUMBER : VL70-000140C -000202C -000205A
-000200B -000203

DIMENSIONS .

FULL SCALE

MODEL SCALE

Length (OML: Fwd Sta. X ₀ =235)	In. <u>1293.3</u>	<u>5.173</u>
Length (IML: Fwd Sta. X ₀ =238)	In. <u>1290.3</u>	<u>5.161</u>
Max. Width (@ X ₀ = 1528.3)	In. <u>264.0</u>	<u>1.056</u>
Max Depth (@ X = 1464)	In. <u>250.0</u>	<u>1.000</u>
Fineness Ratio, (OML Length/Max. Width)	<u>4.899</u>	<u>4.899</u>
Area - Ft ²	<u> </u>	<u> </u>
Max. Cross-Sectional	<u>340.885</u>	<u>0.0055</u>
Planform	<u> </u>	<u> </u>
Wetted	<u> </u>	<u> </u>
Base	<u> </u>	<u> </u>

TABLE III (CONT'D)

MODEL COMPONENT : CANOPY - C12

GENERAL DESCRIPTION : Configuration 140C orbiter canopy vehicle
cabin No. 31 updated to MCR 200-R₄. Used with fuselage B₆₂.

MODEL SCALE: 0.004

DRAWING NUMBER : VL70-000140C -000202B -000204

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length ($X_0 = 434.643$ to 573) In.	<u>143.357</u>	<u>0.573</u>
Max Width (@ $X_0 = 513.127$) In.	<u>152.412</u>	<u>0.610</u>
Max Depth ($Z_0 = 501$ to 449.3) In.	<u>51.61</u>	<u>0.206</u>
Fineness Ratio	_____	_____
Area	_____	_____
Max. Cross-Sectional	_____	_____
Planform	_____	_____
Wetted	_____	_____
Base	_____	_____

TABLE III (CONT'D)

MODEL COMPONENT: ELEVON - E₄₃

GENERAL DESCRIPTION: Configuration 140A 'B orbiter elevons.

DATA are for one side, used on 74-0 model with W₁₀₀. E₄₃ is 6" F.S. straightslotted gap version of E₂₄, gaps are at elevon 'body flare juncture and atY₀ = 311.0

MODEL SCALE: 0.004

DRAWING NUMBER: VL70-000200-006089-006092
R90006 Lockheed Missile & Space Co., Huntsville, Ala.DIMENSIONS:

	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area - Ft ²	<u>210.0</u>	<u>0.003</u>
Span (equivalent). In.	<u>349.2</u>	<u>1.397</u>
Inb'd equivalent chord. In.	<u>118.004</u>	<u>0.472</u>
Outb'd equivalent chord. In.	<u>55.192</u>	<u>0.221</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.2096</u>	<u>0.2096</u>
At Outb'd equiv. chord	<u>0.4004</u>	<u>0.4004</u>
Sweep Back Angles, degrees		
Leading Edge	<u>0.00</u>	<u>0.00</u>
Tailing Edge	<u>-10.056</u>	<u>-10.056</u>
Hingeline Area Moment (Product of area & c) ³ Ft ³	<u>0.00</u>	<u>0.00</u>
Mean Aerodynamic Chord. In.	<u>90.7</u>	<u>0.363</u>

TABLE III (CONT'D)

MODEL COMPONENT : BODY FLAP - F₁₀

GENERAL DESCRIPTION : Configuration 14OC body flap. Hingeline located at $X_0 = 1532$, $Z_0 = 287$.

MODEL SCALE: 0.004

DRAWING NUMBER : VL70-00014OC, VL70-355114

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length ($X_0 = 1525.5$ to 1613) In.	<u>87.10</u>	<u>0.350</u>
Max Width (@ L.E., $X_0 = 1525.5$) In.	<u>256.00</u>	<u>1.024</u>
Max Depth ($Z_0 = 1532$) In.	<u>19.798</u>	<u>0.792</u>
Fineness Ratio	<u>—</u>	<u>—</u>
Area - Ft. ²	<u>—</u>	<u>—</u>
Max. Cross-Sectional (@ H. L.)	<u>35.196</u>	<u>0.00056</u>
Planform	<u>135.00</u>	<u>0.0022</u>
Wetted	<u>—</u>	<u>—</u>
Base (@ $X_0 = 1613$)	<u>4.89</u>	<u>0.000078</u>

TABLE III (CONT'D)

MODEL COMPONENT : OMS POD - M₁₄GENERAL DESCRIPTION : Preliminary IML version of short OMS pod.(First used on 0.015 scale Model 3A-0 for test No. OA83).MODEL SCALE: 004DRAWING NUMBER : VL70-008457

DIMENSIONS : (For 1 or 2 sides)	FULL SCALE	MODEL SCALE
Length (OMS Fwd Sta $X_0 = 1311$), In.	<u>254.0</u>	<u>1.036</u>
Max Width (@ $X_0 = 1511$) In.	<u>135.6</u>	<u>0.5624</u>
Max Depth (@ $X_0 = 1511$) In.	<u>73.6</u>	<u>0.2944</u>
Fineness Ratio	<u>2.54080</u>	<u>2.54080</u>
Area - Ft ²	_____	_____
Max. Cross-Sectional	<u>54.507</u>	<u>0.00087</u>
Planform	_____	_____
Wetted	_____	_____
Base	_____	_____

TABLE III (CONT'D)

MODEL COMPONENT: VERTICAL - V₈

GENERAL DESCRIPTION: Configuration 140C orbiter vertical tail (identical to configuration 140A 'B vertical tail).

MODEL SCALE: 0.004

DRAWING NUMBER: VL70-000140C -000146R

DIMENSIONS:

FULL SCALEMODEL SCALE

TOTAL DATA

Area (Theo) - Ft ²	<u>413.253</u>	<u>0.0068</u>
Planform	<u>315.72</u>	<u>1.263</u>
Span (Theo) - In.	<u>1.675</u>	<u>1.675</u>
Aspect Ratio	<u>0.507</u>	<u>0.507</u>
Rate of Taper	<u>0.404</u>	<u>0.404</u>
Sweep-Back Angles, Deg.:		
Leading Edge	<u>45.000</u>	<u>45.000</u>
Trailing Edge	<u>26.2</u>	<u>26.2</u>
0.25 Element Line	<u>41.13</u>	<u>41.13</u>

Chords:

Root (Theo) WP	<u>268.50</u>	<u>1.074</u>
Tip (Theo) WP	<u>108.47</u>	<u>0.431</u>
M.C.	<u>199.81</u>	<u>0.799</u>
Fus. Sta. of .25 MAC	<u>1463.35</u>	<u>5.853</u>
W.P. of .25 MAC	<u>635.52</u>	<u>2.542</u>
B.L. of .25 MAC	<u>0.0</u>	<u>0.0</u>

Airfoil Section

Leading Wedge Angle - Deg.	<u>10.000</u>	<u>10.000</u>
Trailing Wedge Angle - Deg.	<u>14.92</u>	<u>14.92</u>
Leading Edge Radius	<u>2.00</u>	<u>0.008</u>

Void Area

13.170.00021

Blanketed Area

0.00.0

TABLE III (CONT'D)

MODEL COMPONENT: RUDDER - R₅GENERAL DESCRIPTION: Configuration 140C orbiter rudder (identical to Configuration 140A 'B' rudder).MODEL SCALE: 0.004DRAWING NUMBER: VL70-000146B -000095

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area - Ft ²	<u>100.15</u>	<u>0.0016</u>
Span (equivalent) . In.	<u>201.00</u>	<u>0.804</u>
Inb'd equivalent chord . In.	<u>91.585</u>	<u>0.366</u>
Outb'd equivalent chord . In.	<u>50.833</u>	<u>0.203</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
At Outb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
Sweep Back Angles, degrees		
Leading Edge	<u>34.83</u>	<u>34.83</u>
Tailing Edge	<u>26.25</u>	<u>26.25</u>
Hingeline (Product of Area & c)	<u>34.83</u>	<u>34.83</u>
Area Moment (Normal to hingeline) . Ft. ³	<u>610.92</u>	<u>0.000039</u>
Mean Aerodynamic Chord . In.	<u>73.2</u>	<u>0.293</u>

TABLE III. (Concluded)

MODEL COMPONENT: WING-W,27

GENERAL DESCRIPTION: Configuration 140C orbiter wing, MCR 200-R, similar to
 140A 'B wind W₁₁₆ but with refinements: improved wing-boot-midbody fairing
 (.X₀ = 940 to X₀ = 1040).

MODEL SCALE: 0.001

TEST NO.	DWG. NO. VL70-000140C, -000200B	
DIMENSIONS:		
	FULL-SCALE	MODEL SCALE
<u>TOTAL DATA</u>		
Area (Theo.) Ft ²		
Planform	2690.00	0.043
Span (Theo) In.	936.68	3.747
Aspect Ratio	2.265	2.265
Rate of Taper	1.177	1.177
Taper Ratio	0.200	0.200
Dihedral Angle, degrees	3.500	3.500
Incidence Angle, degrees	0.500	0.500
Aerodynamic Twist, degrees	3.000	3.000
Sweep Back Angles, degrees		
Leading Edge	34.000	45.000
Trailing Edge	10.056	10.056
0.25 Element Line	35.209	35.209
Chords:		
Root (Theo) B.P.O.O.	689.24	2.757
Tip (Theo) B.P.	137.85	0.551
MAC	474.81	1.899
Fus. Sta. of .25 MAC	1136.83	4.547
W.P. of .25 MAC	290.58	1.162
B.L. of .25 MAC	182.13	0.729
<u>EXPOSED DATA</u>		
Area (Theo) Ft ²		
Span, (Theo) In. BP108	1751.50	7.006
Aspect Ratio	720.68	2.883
Taper Ratio	2.059	2.059
Chords		
Root BP108	0.245	0.245
Tip $\frac{b}{2}$	562.09	2.248
MAC	137.85	0.551
Fus. Sta. of .25 MAC	392.83	1.531
W.P. of .25 MAC	1185.98	4.744
B.L. of .25 MAC	294.30	1.177
Airfoil Section (Rockwell Mod NAS/L) XXXX-64	251.77	1.007
Root $\frac{b}{2}$	0.113	0.113
Tip $\frac{b}{2}$	0.120	0.120
Data for (1) or (2) Sides		
Leading Edge Cuff		
Planform Area Ft ²	113.10	0.0018
Leading Edge Intersects Fus M. L. @ Sta	500.00	2.000
Leading Edge Intersects Wing @ Sta	1024.00	4.096

Notes:

1. Positive directions of force coefficients, moment coefficients, and angles are indicated by arrows
2. For clarity, origins of wind and stability axes have been displaced from the center of gravity

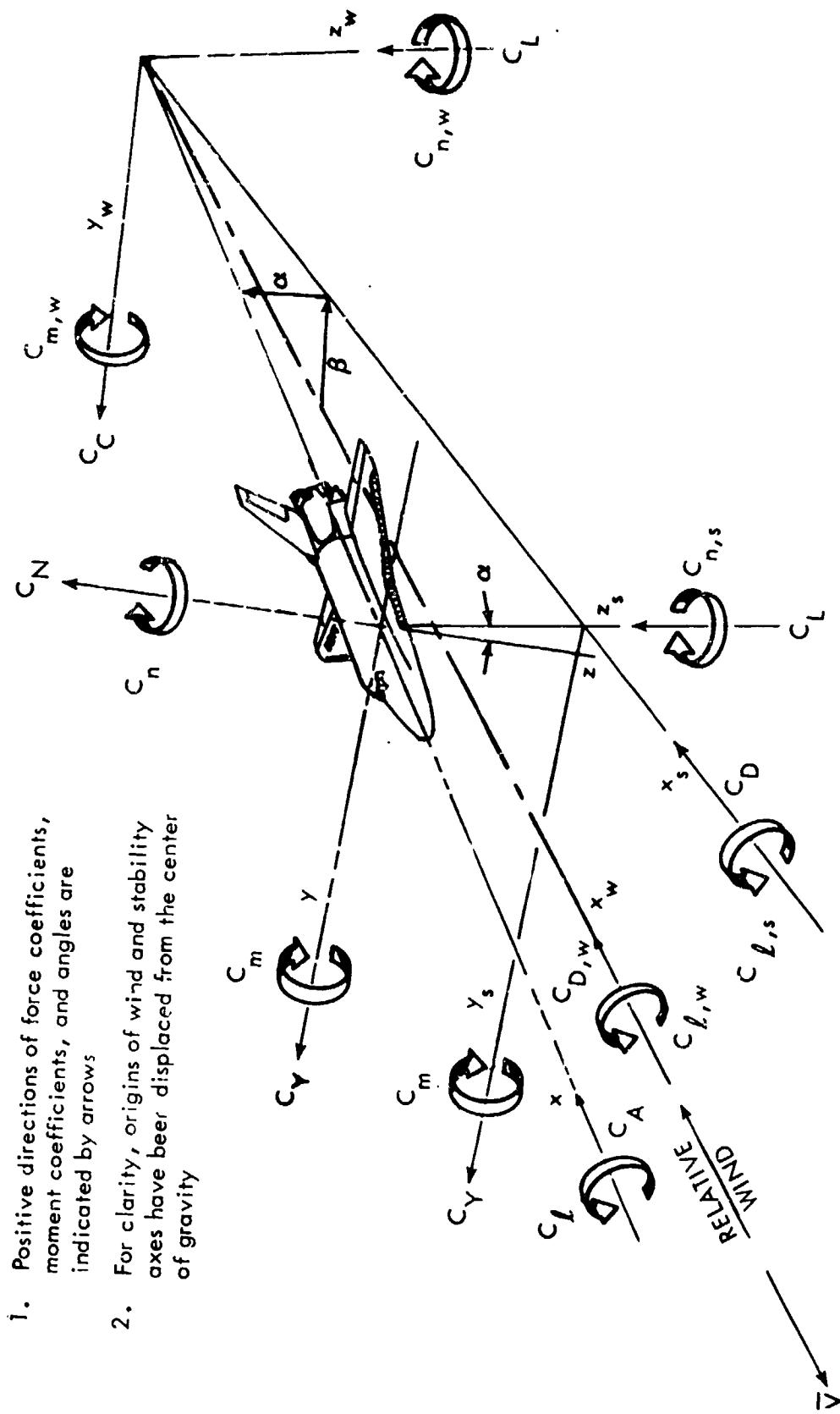


Figure 1. - Axis systems.

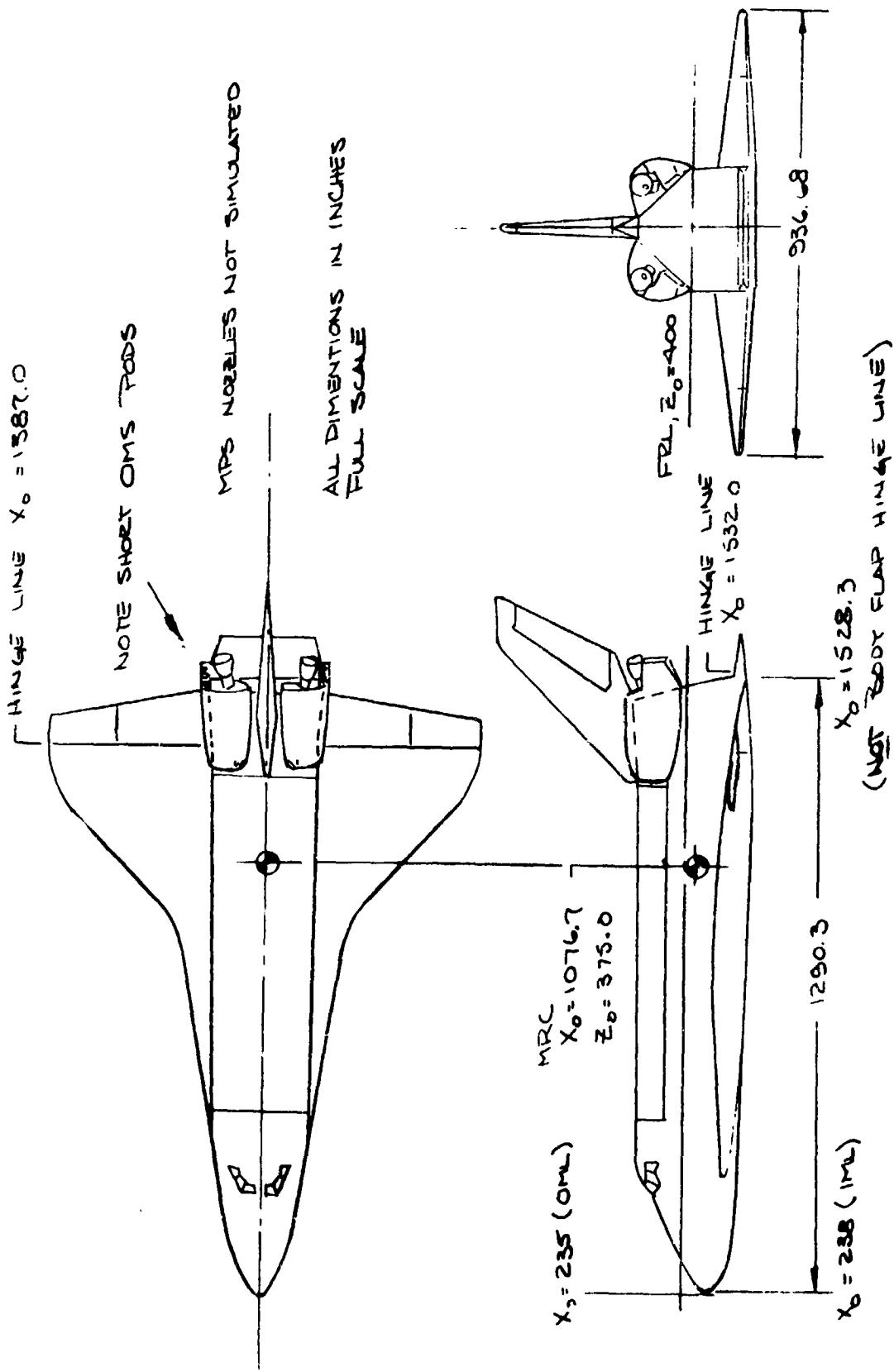
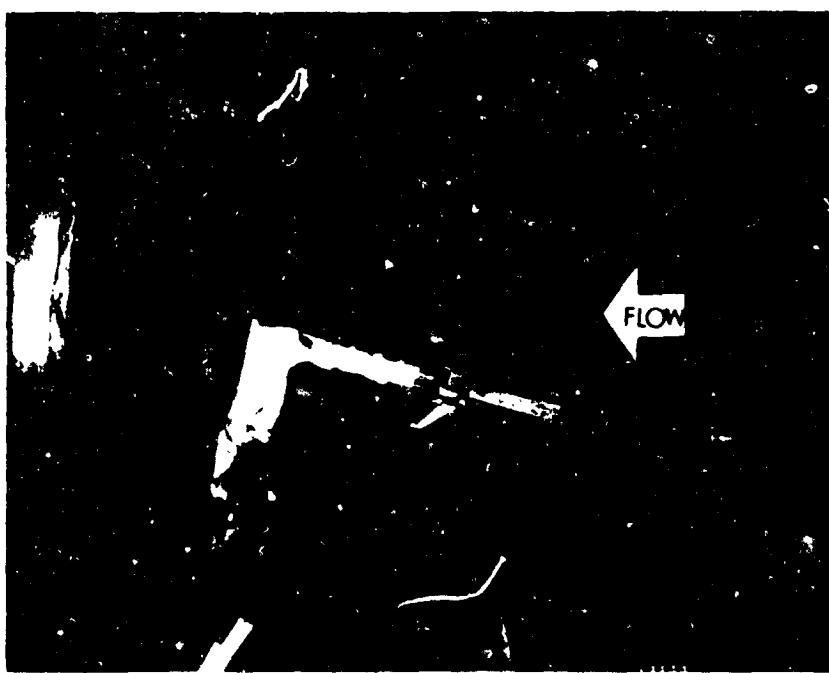


Figure 2. - 140C modified Orbiter for test OA89



a. Test Section with Model Injected, 45° Bent Sting



b. 74-0 Model on 45° Sting

Figure 3. - Model photographs.

DATA FIGURES

DATA SET SYMBOL	CONFIGURATION	DESCRIPTION
[R00001]	D	M19 N1 I-3015A-89
[R00002]		M19 N1 I-3015A-89
[R00003]		M19 N2 I-3015A-89
[R00004]		M19 N3 I-3015A-89
[R00005]		M19 N4 I-3015A-89

ELEVATOR	ALTRON	BDFLAP	SPDRK	REFERENCE INFORMATION
200	.000	.000	55.000	S&F
200	.000	.000	55.000	S&F
200	.000	.000	55.000	S&F
-30.000	.000	.000	55.000	S&F

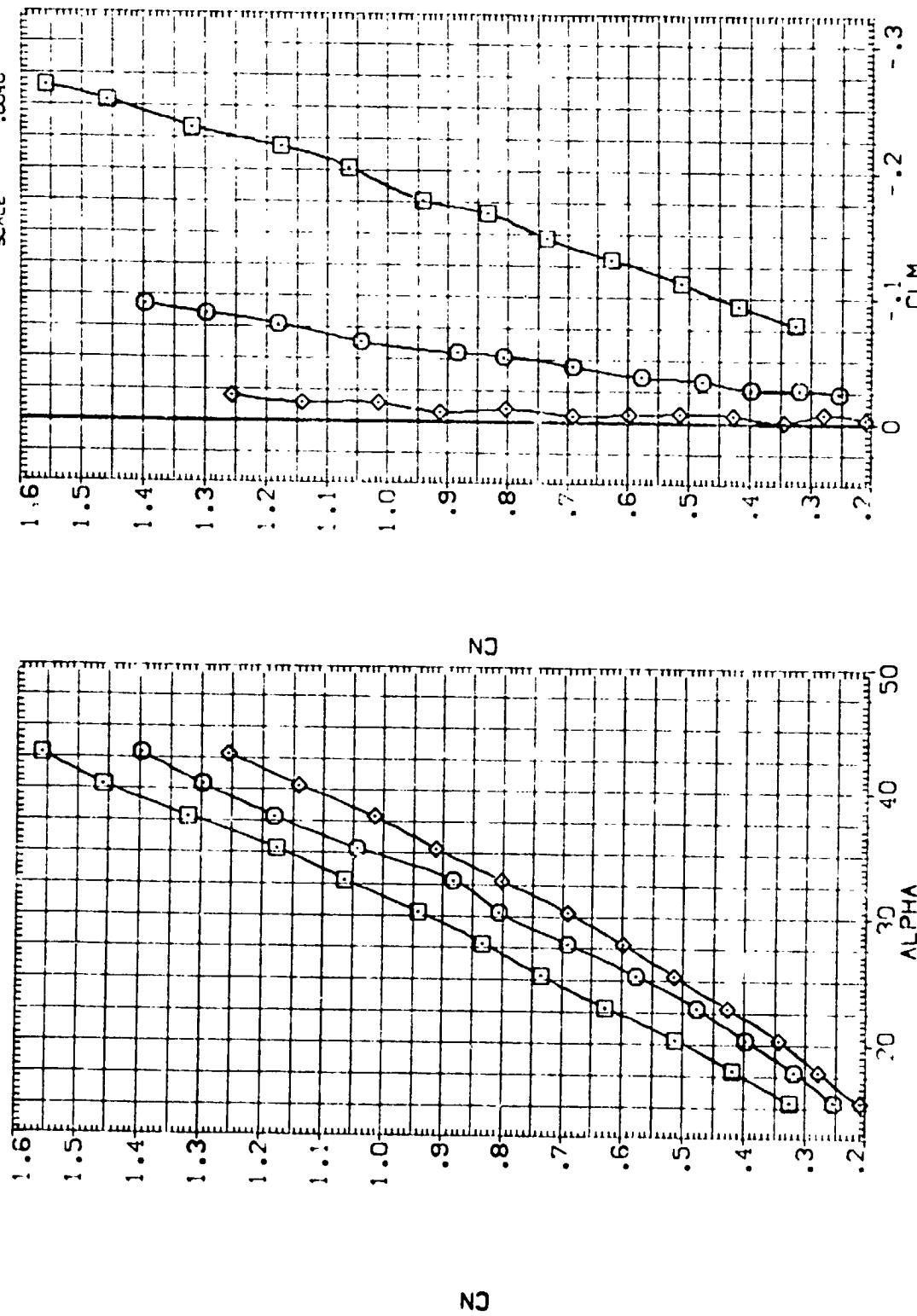


FIGURE 4 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHARACTERISTICS

DATA SET SYMBOL CONFIGURATION DESCRIPTION

RA00001	M19 N.1.-30 [DA-89] {V12E13} [V12E13] [V12E13]
RA00002	M19 N.1.-30 [DA-89] {V12E13} [V12E13] [V12E13]
RA00003	M19 N.1.-30 [DA-89] {V12E13} [V12E13] [V12E13]

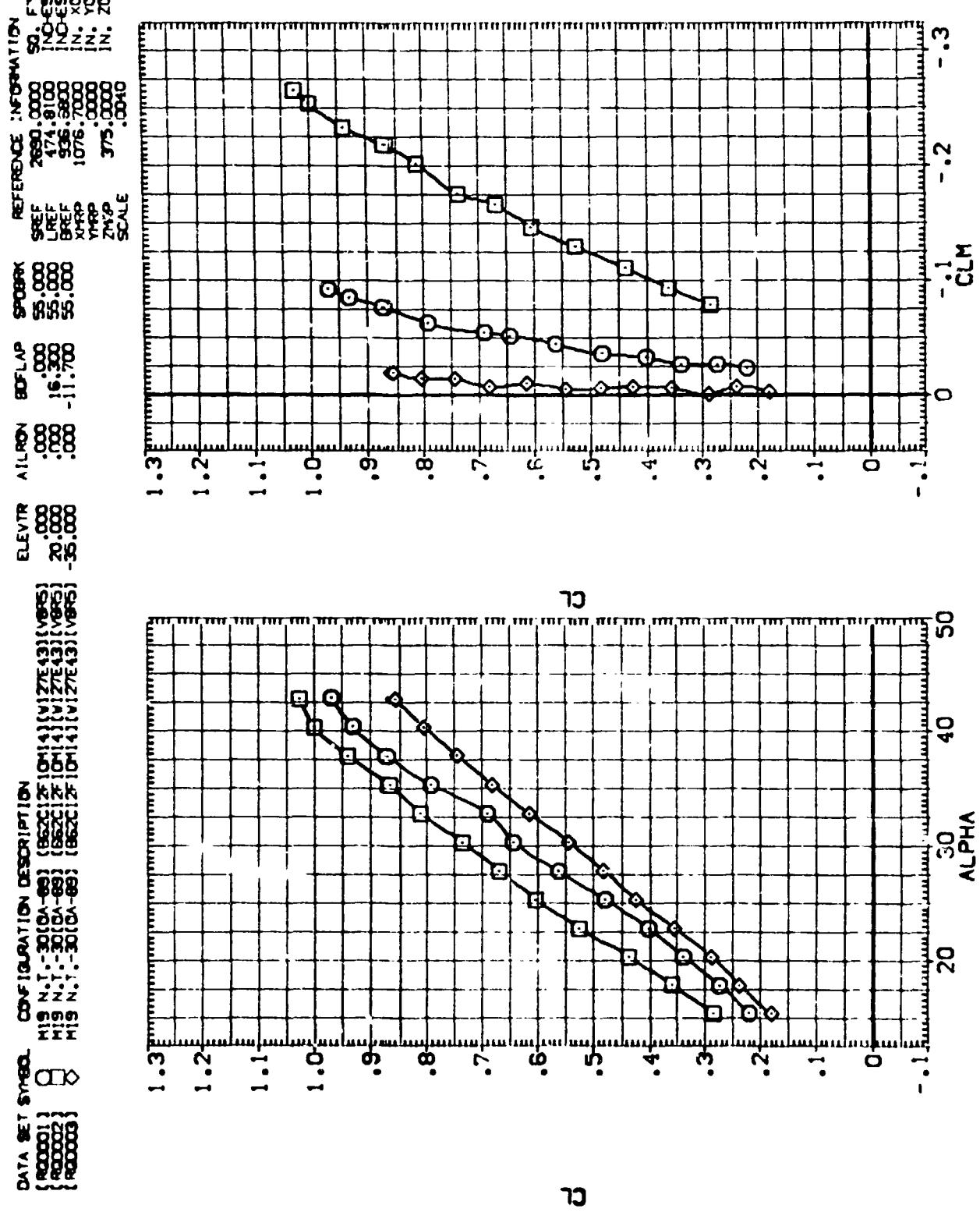


FIGURE 4 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHART(45DEG STING)
 $\alpha_{MACH} = 19.80$



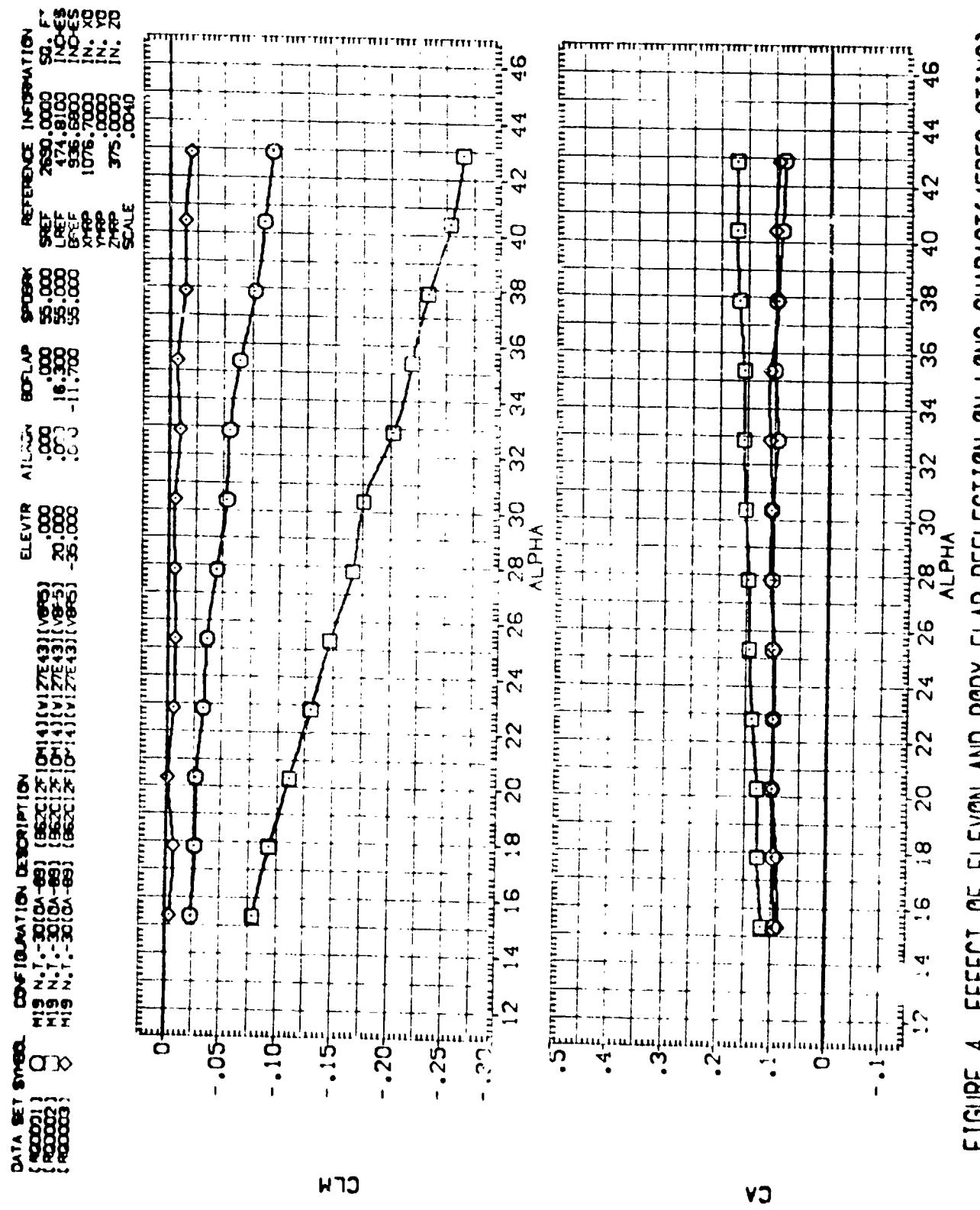


FIGURE 4 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHARACT(45DEG STING)
 $(\alpha)_MACH = 19.80$

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DATA SET SPEC. CONFIGURATION DESCRIPTION
 DATA SET 1: MIG N. 1 - 30 [0A-0B] (85C) 21 101 111 [V127E43] (V125)
 DATA SET 2: MIG N. 1 - 30 [0A-0B] (85C) 21 101 111 [V127E43] (V125)
 DATA SET 3: MIG N. 1 - 30 [0A-0B] (85C) 21 101 111 [V127E43] (V125)

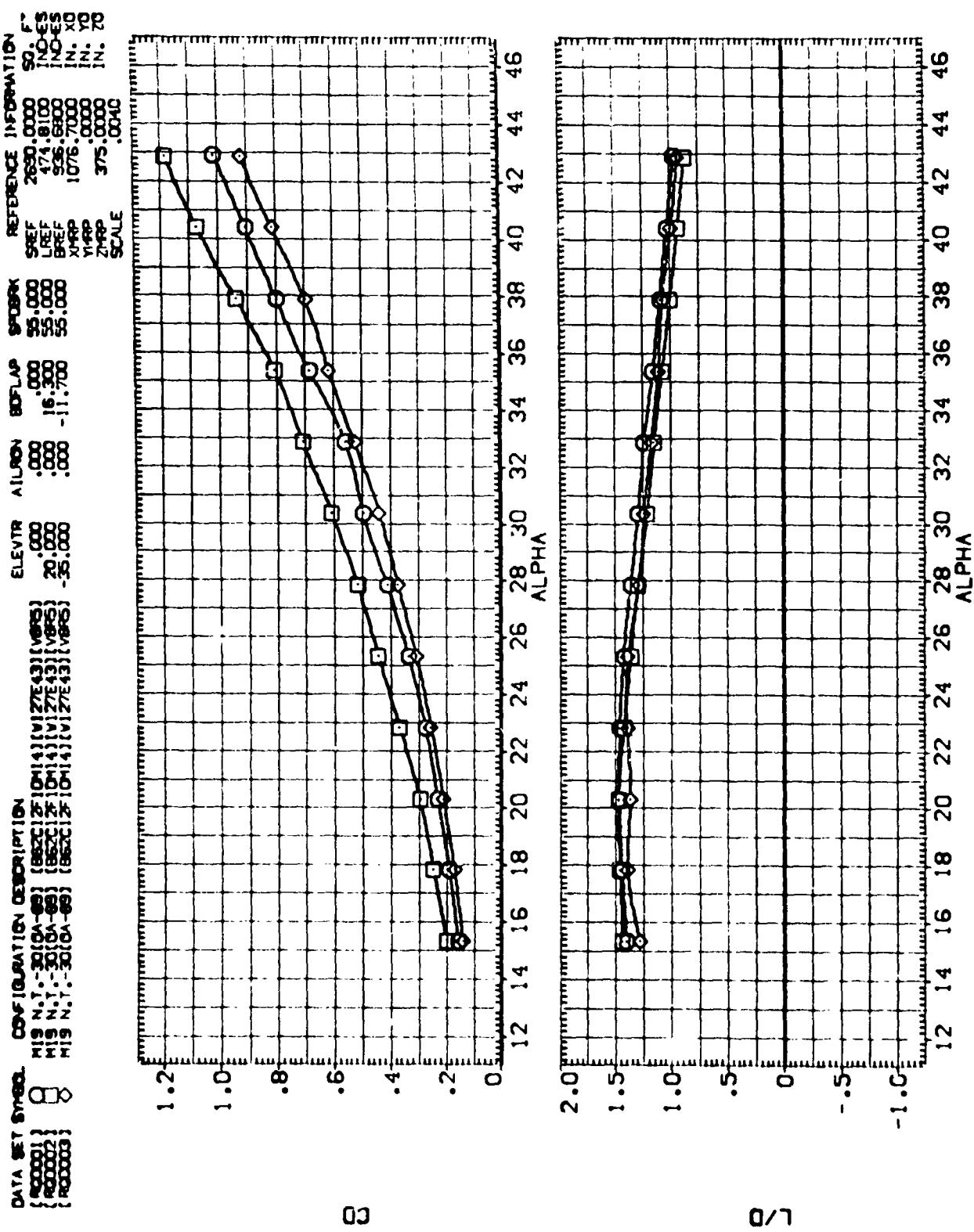


FIGURE 4 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON L/D CHARACTERISTICS
 CA/MACH = 1.980

DATA SET SYMBOL		CONFIGURATION DESCRIPTION		ELE / TR		AILRDN		BDFLAP		SPDRK		REFERENCE INFORMATION	
R00008	Q	H19 N. 1.-31	(DA-68) (B62C 2F 1OM 143) (V127E 43) (V85)	.000	.000	.000	.000	.000	.000	.000	.000	SREF	2690 .0000 .50
R00007	Q	H19 N. 1.-31	(DA-68) (B62C 2F 1OM 143) (V127E 43) (V85)	.000	.000	.000	.000	.000	.000	.000	.000	LREF	474 .6100 .50
R00008	X	H19 N. 1.-31	(DA-68) (B62C 2F 1OM 143) (V127E 43) (V85)	.000	.000	.000	.000	.000	.000	.000	.000	BREF	536 .6800 .50
R00009	X	H19 N. 1.-31	(DA-68) (B62C 2F 1OM 143) (V127E 43) (V85)	.000	.000	.000	.000	.000	.000	.000	.000	XHPP	1076 .7000 .50
												YHPP	375 .8000 .50
												ZHPP	.0040 .20
												SCALE	

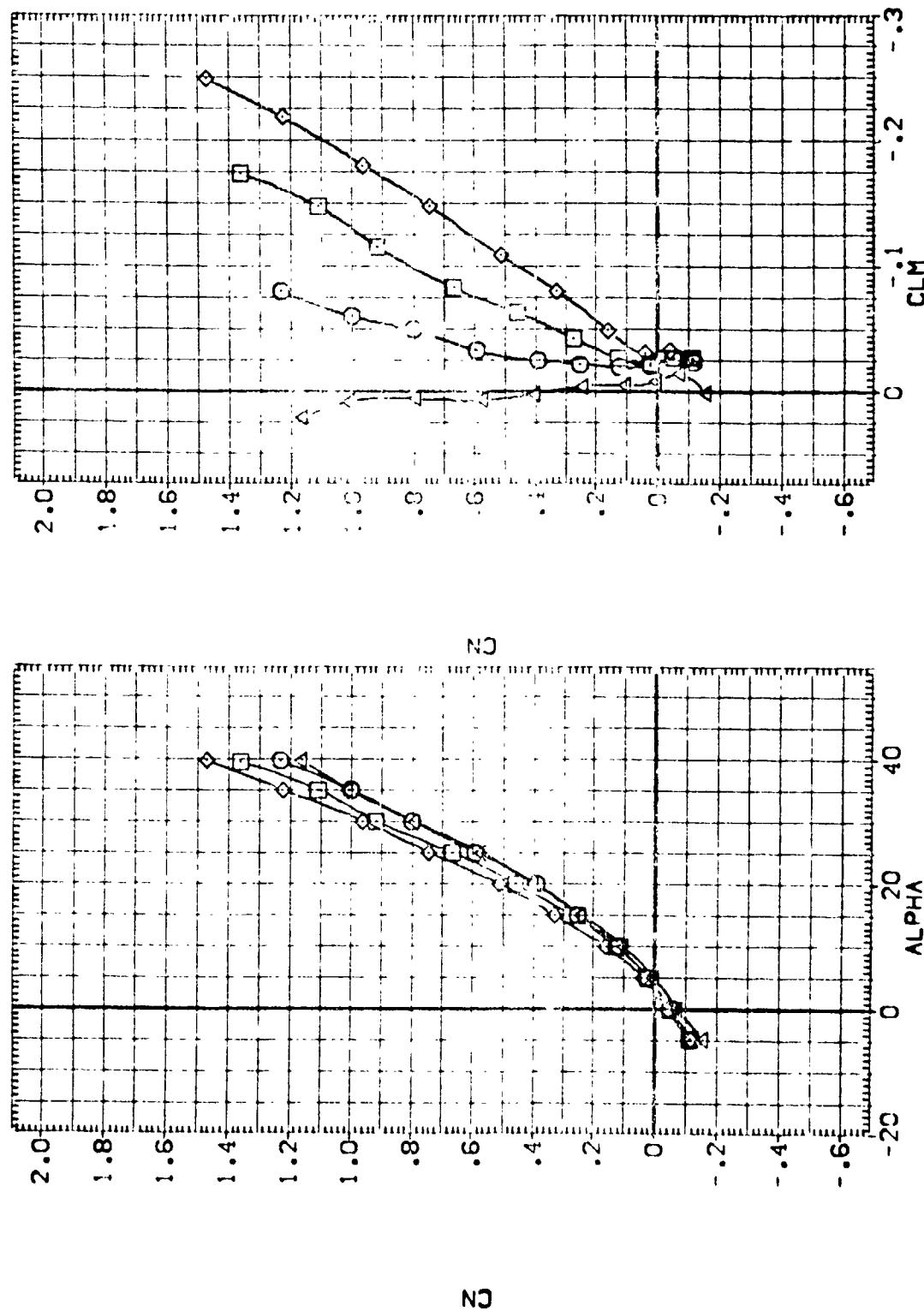


FIGURE 5 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHARACT (25DEG STING)
 $C_{AJMACH} = 19.80$

DATA SET NUMBER: CONFIGURATION DESCRIPTION: M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5)

1000002	M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5)
1000007	M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5)
1000008	M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5)
1000009	M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5)

LEVTR .000 ALTDYN .000 BOFLAP .000 SPDRK 55.000 REF 2600.000 90. FT
 M13 N.1.-310A-20 [B22C12] [B22C13] [B22C14] [V127E43] (VER5) LREF 474.8100 NO-ES
 10.000 .000 16.300 55.000 BREF 936.6900 NO-ES
 20.000 .000 -11.700 55.000 XREF 1076.7000 NO-ES
 40.000 .000 0.000 55.000 YREF 375.0000 NO-ES
 SCALE .0040 ZREF

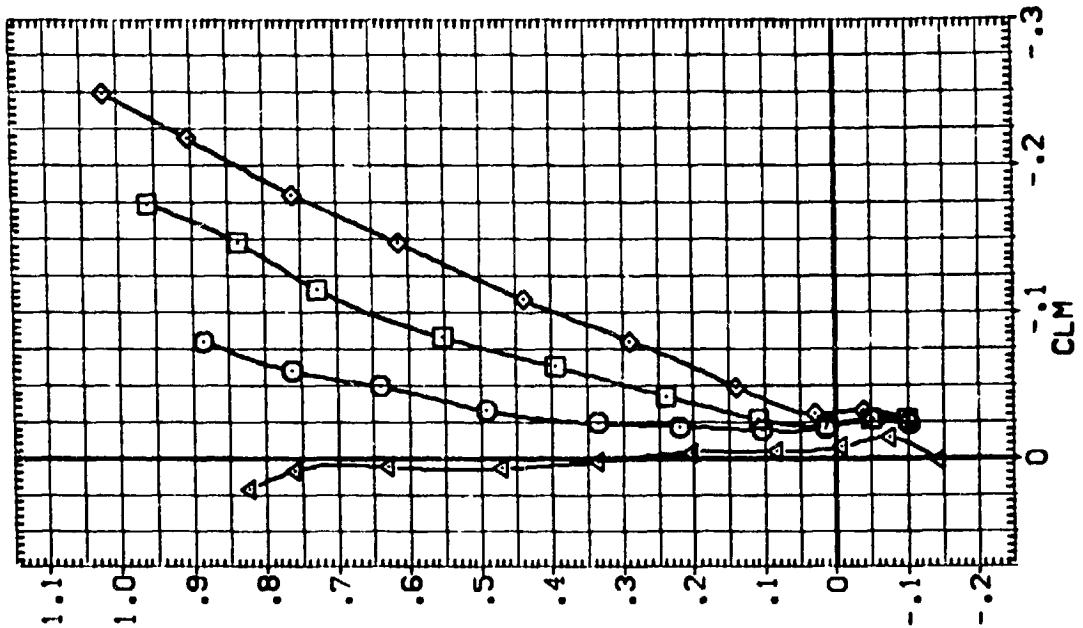
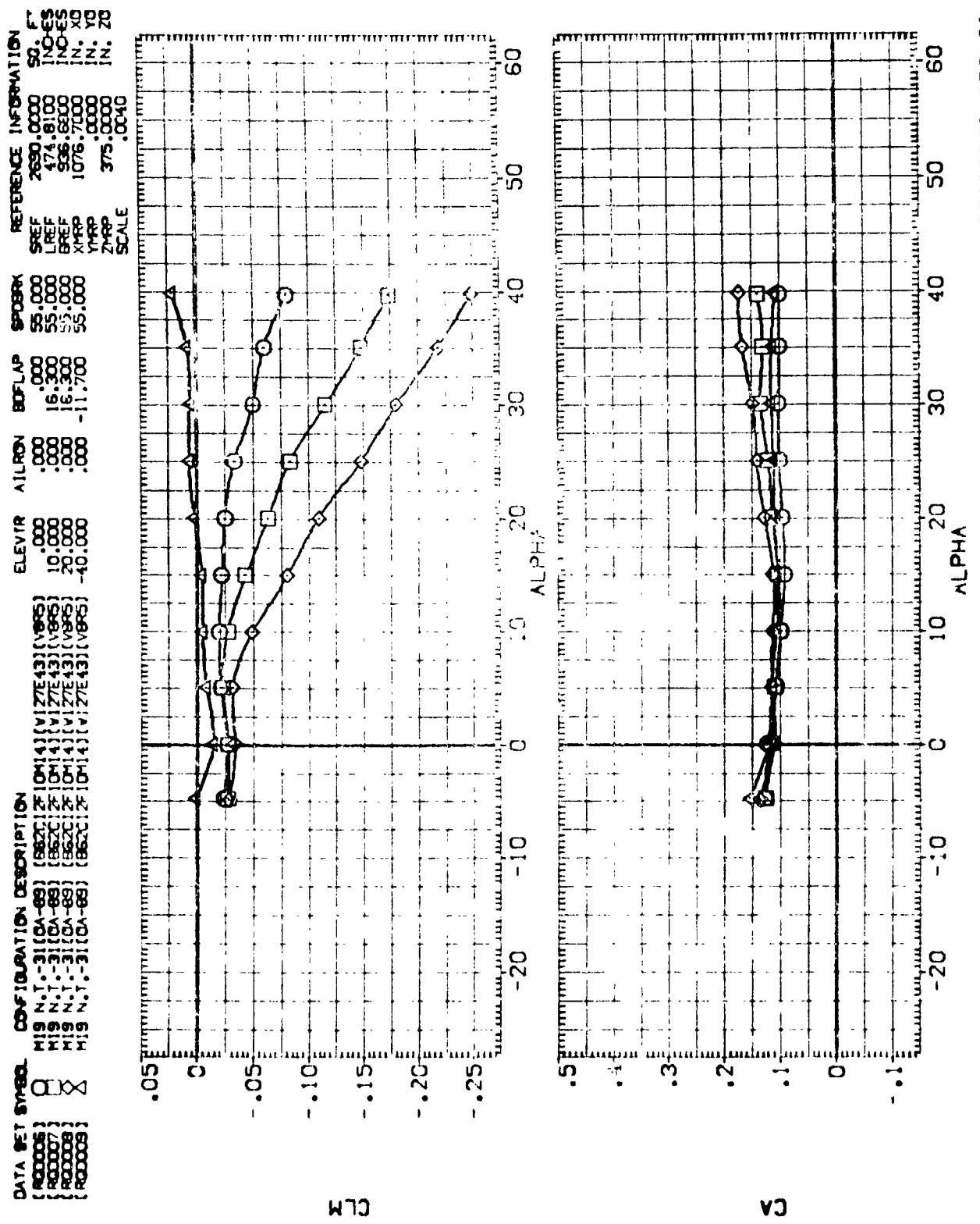


FIGURE 5 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHARACT(25DEG STING)
 CA(MACH) = 19.80
 PAGE 6





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OF POOR QUALITY

FIGURE 5 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LONG CHARACTER (25DEG STING)
 $(\text{A}_\infty \text{MACH} = 19.80)$

DATA SET SYMBOL CONFIGURATION DESCRIPTION
 R00006 H19 N,T,-3[OA,-8] [B52C12][D114][V127E43][V855]
 R00007 H19 N,T,-3[OA,-8] [B52C12][D114][V127E43][V855]
 R00008 H19 N,T,-3[OA,-8] [B52C12][D114][V127E43][V855]
 R00009 H19 N,T,-3[OA,-8] [B52C12][D114][V127E43][V855]

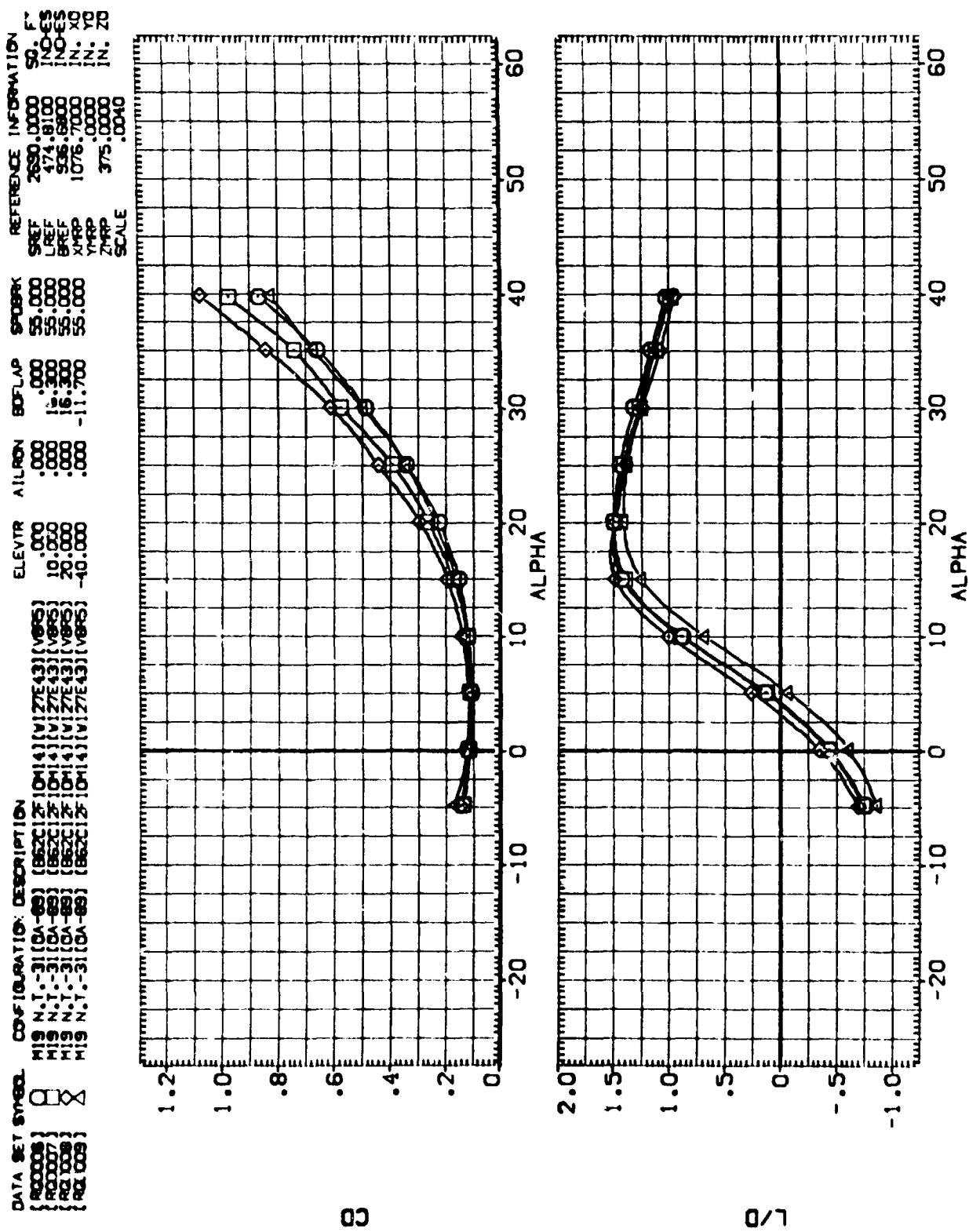
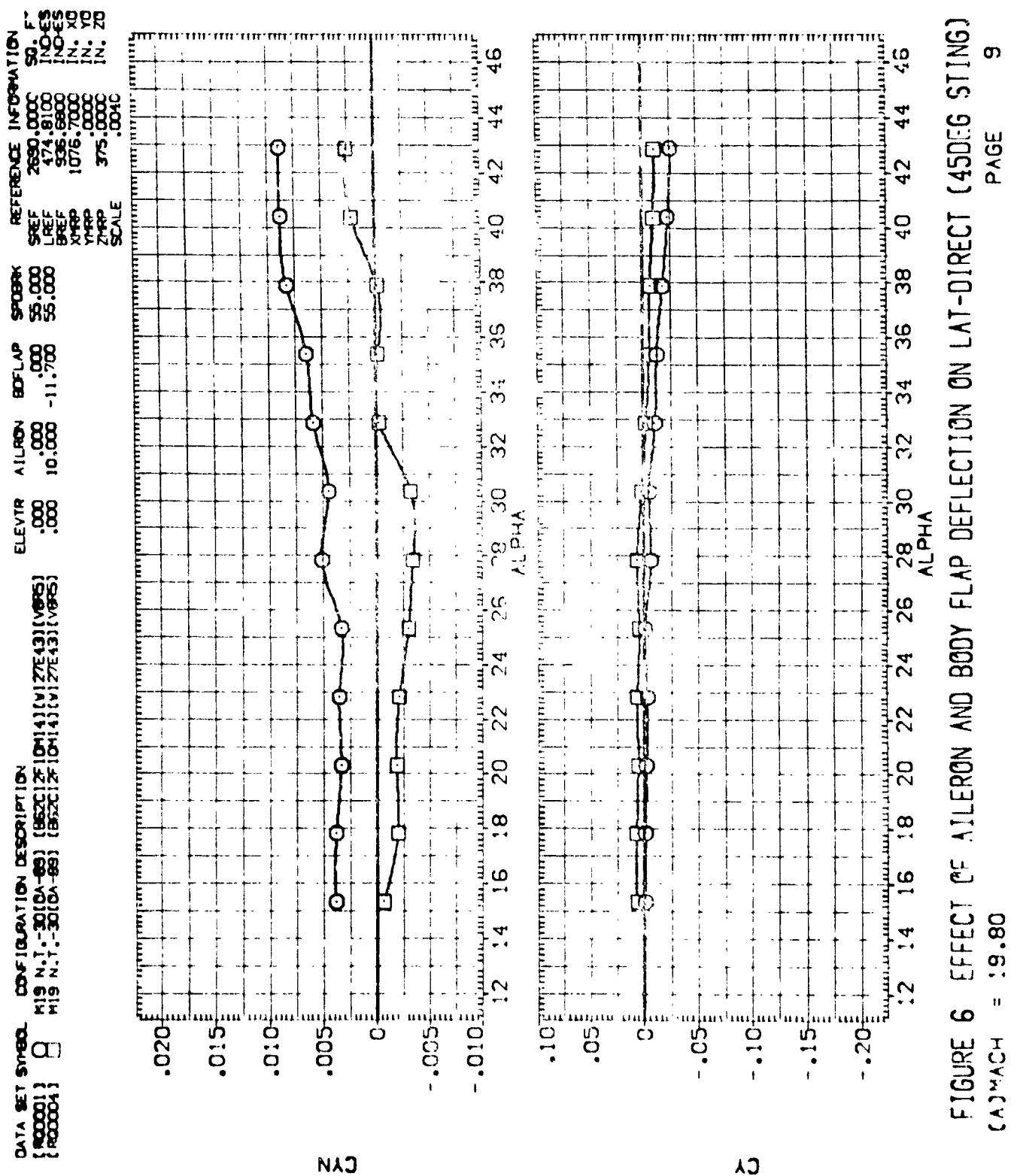


FIGURE 5 EFFECT OF ELEVON AND BODY FLAP DEFLECTION ON LIFT COEFFICIENT (250EG STING)
 CA,MACH = 19.80



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FIGURE 6 EFFECT OF AILERON AND BODY FLAP DEFLECTION ON LAT-DIRECT (45DEG STING)
($MACH = 19.80$)



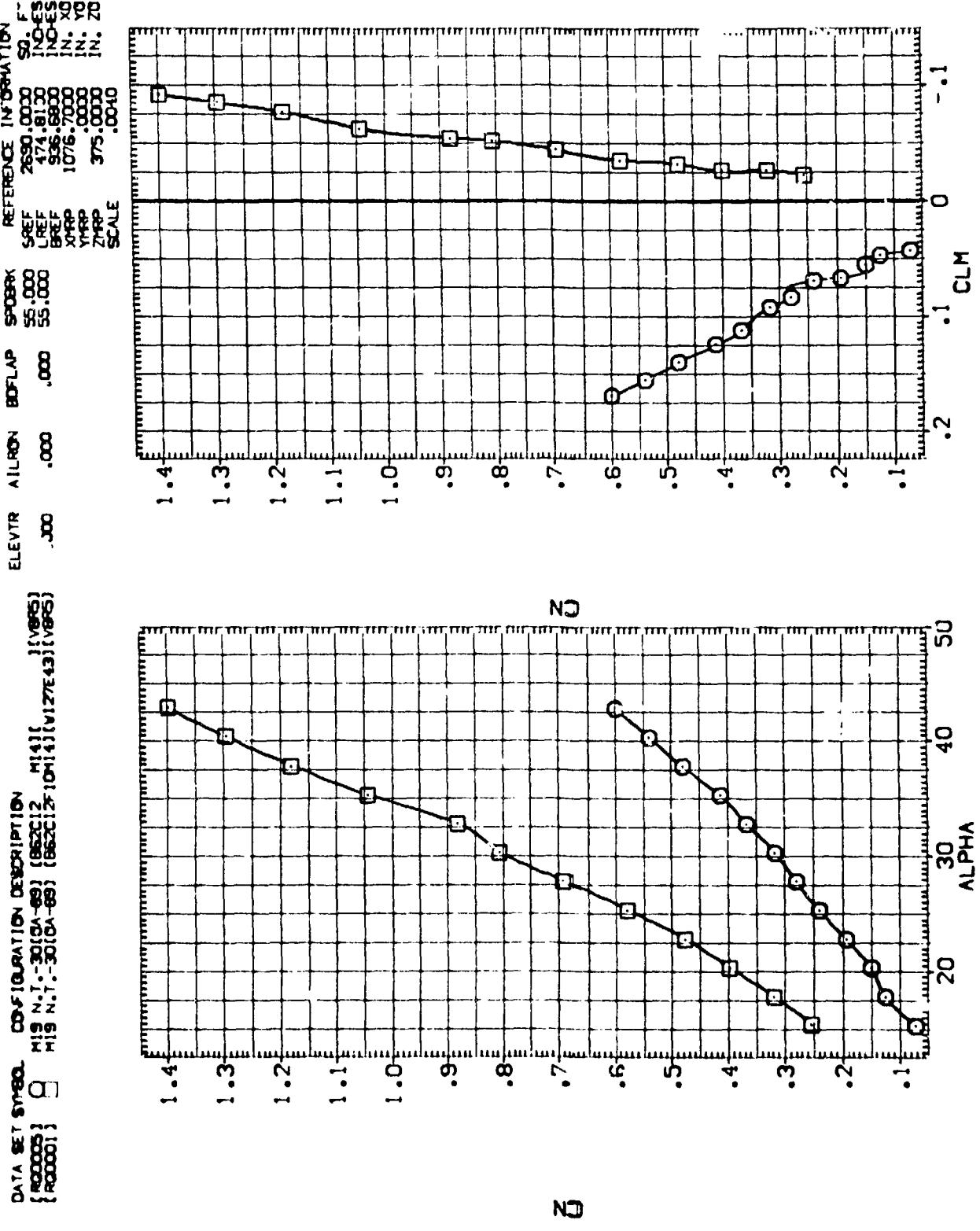


FIGURE 7 EFFECT OF WING AND BODY FLAP ON LONG. CHARACT. (45 DEG. STING)
 CA(MACH) = 19.80

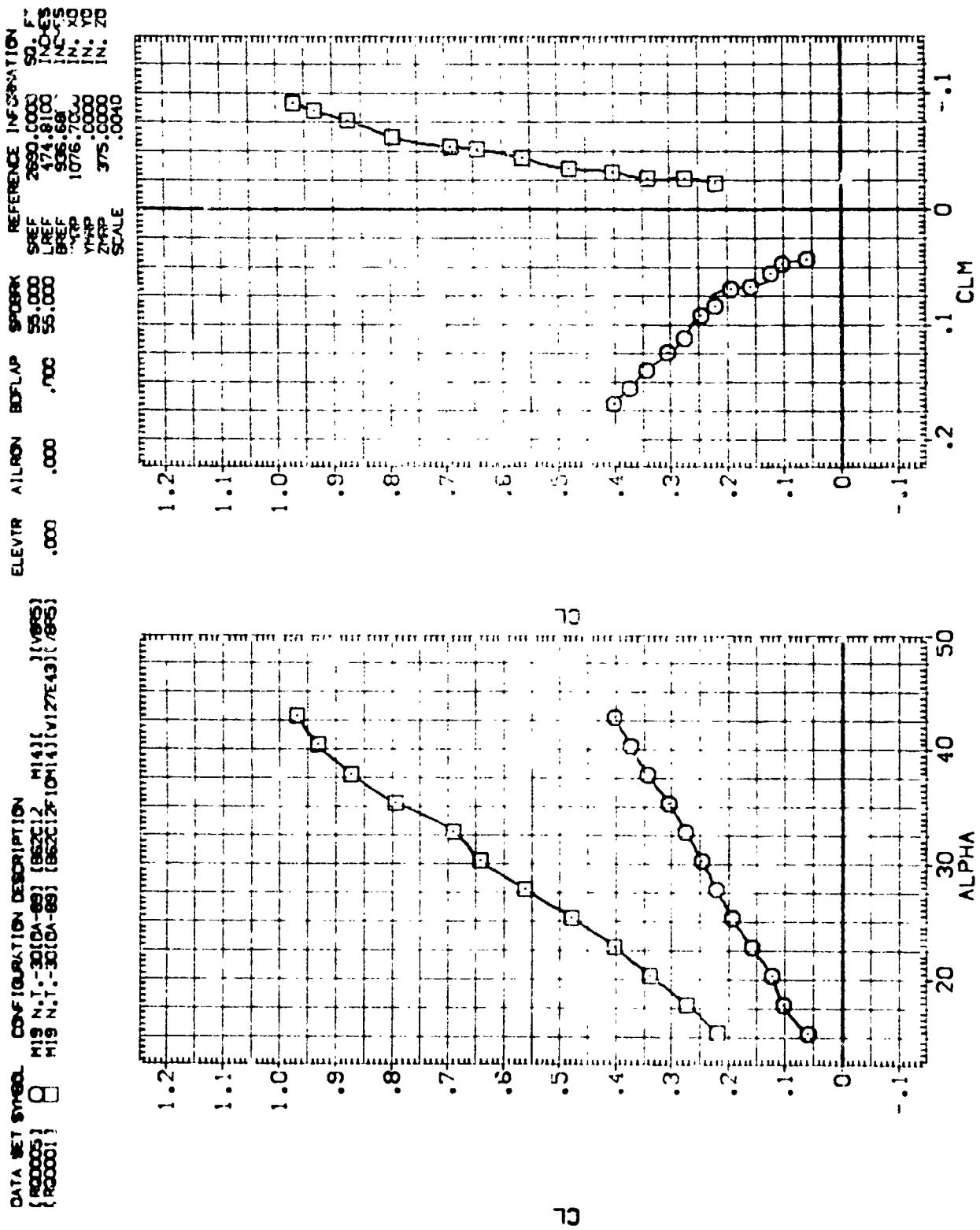


FIGURE 7 EFFECT OF WING AND BODY FLAP ON LONG. CHARACT. (45 DEG. STING! PAC = 18.80

PAC = 11

DATA SET #1
 CONFIGURATION DESCRIPTION: HIG N.1-30[DA-5] [RESC]2[10]14{V12743}{V853}
 REF. 200.0000
 LREF. 474.9100
 SREF. 936.8800
 XTRP. 1076.7000
 YTRP. .0000
 ZTRP. 375.0000
 SCALE .0000

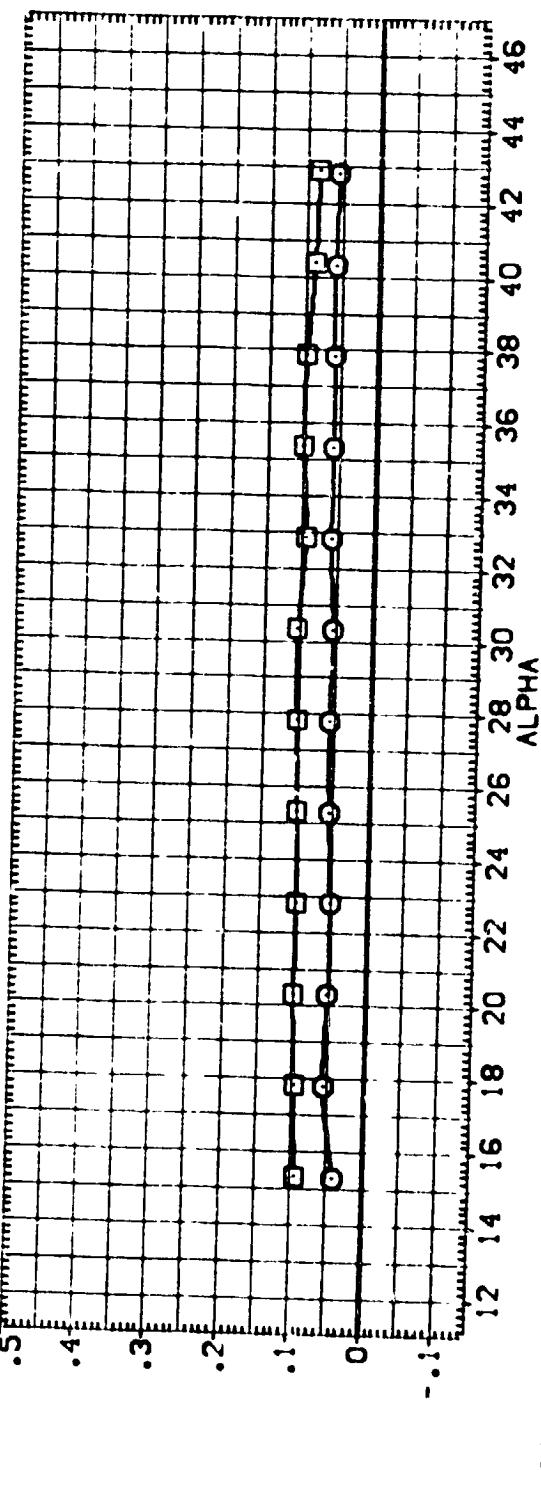
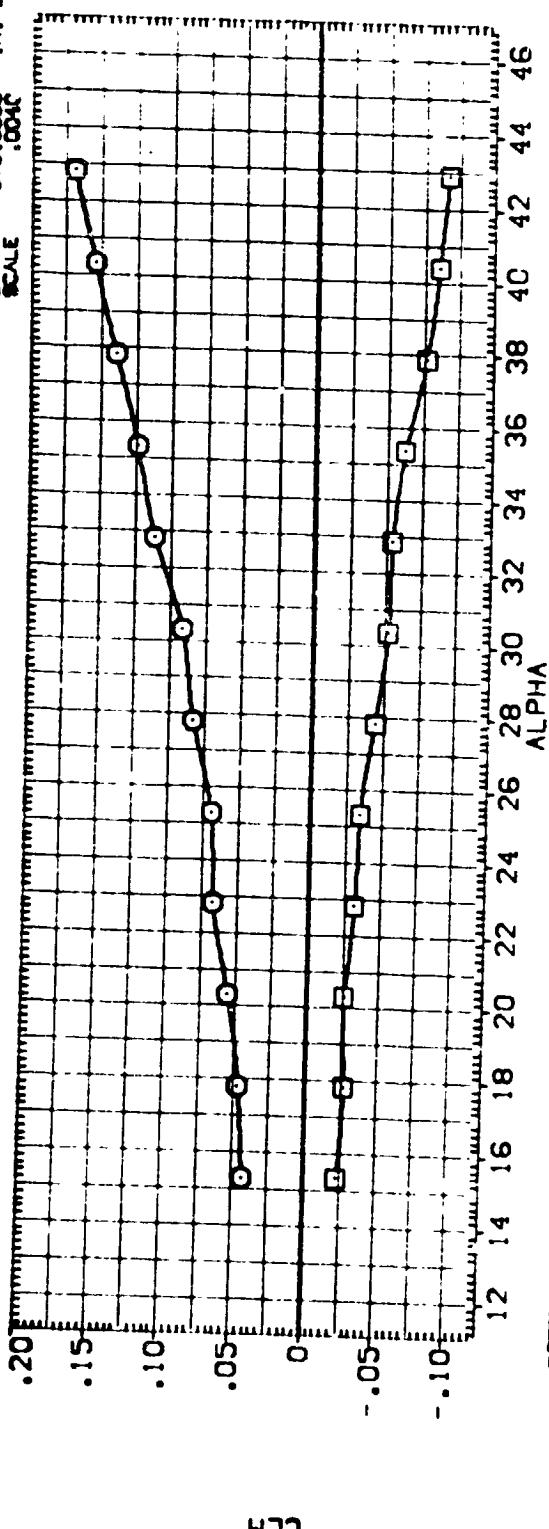


FIGURE 7 EFFECT OF WING AND BODY FLAP ON LONG. CHARACT. (45 DEG. STING)
 $C_{A,MACH} = 19.80$

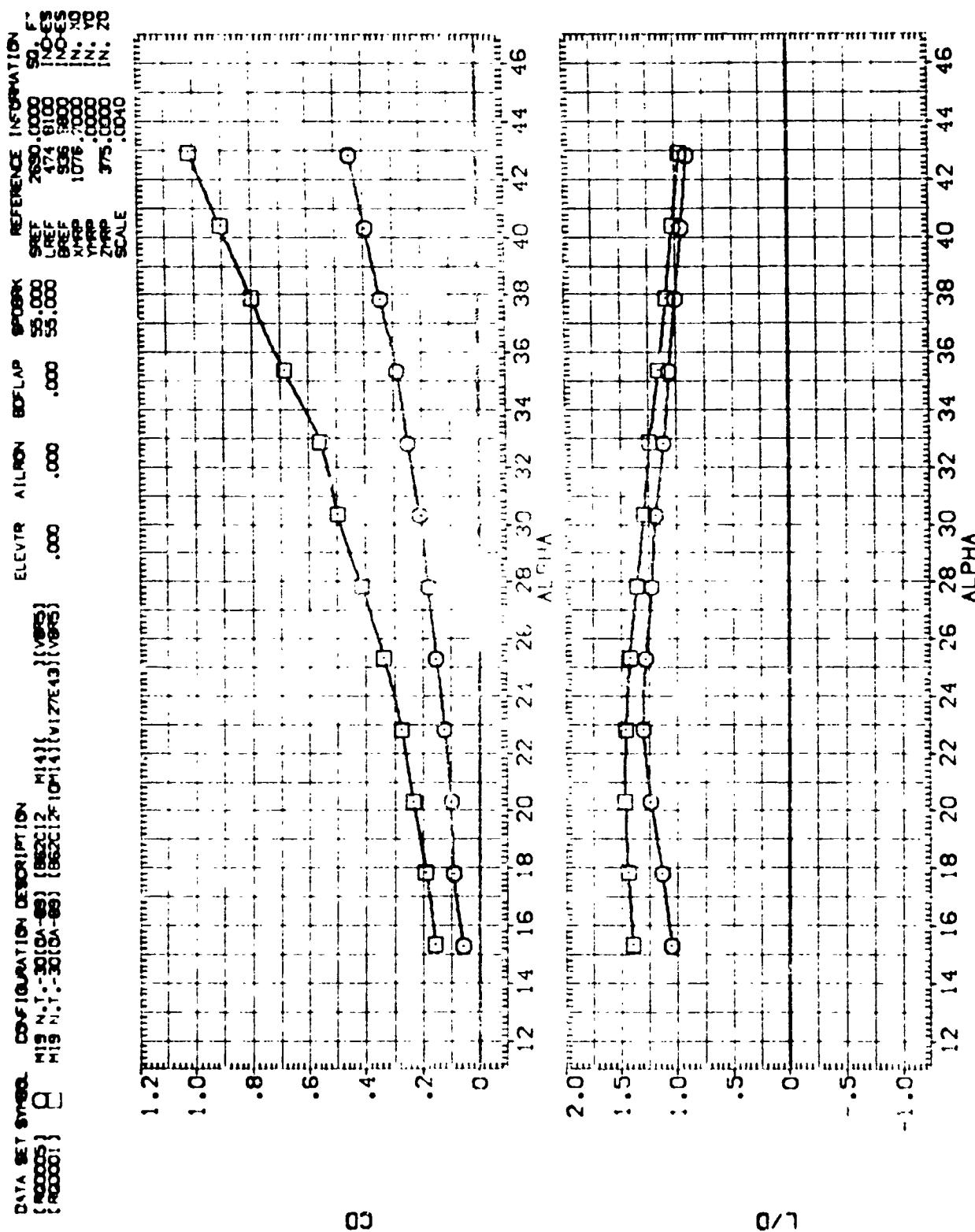


FIGURE 7 EFFECT OF WING AND BODY FLAP ON LONG. CHARACT. (45 DEG. STING)
 (A)MACH = 1.980

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DATA SET SYMBOL CONFIGURATION DESCRIPTION
 { 800001 } MIG N.T.-30[GA-88] [852C12] [M14] [V127E43] (VER5)
 { 800002 } MIG N.T.-31[GA-89] [852C12] [M14] [V127E43] (VER5)

ELEVTR .000 SDFLAP :000 SPDRK 45,000 STING 26,90,000 REF 20, F⁻
 .000 :000 55,000 25,000 LREF 474,8100 NOES
 BREF 9,36,9800 NO-ES
 XHPP 1,78,7000 N: XG
 YHPP .0000 N: ZD
 SCALE .0040

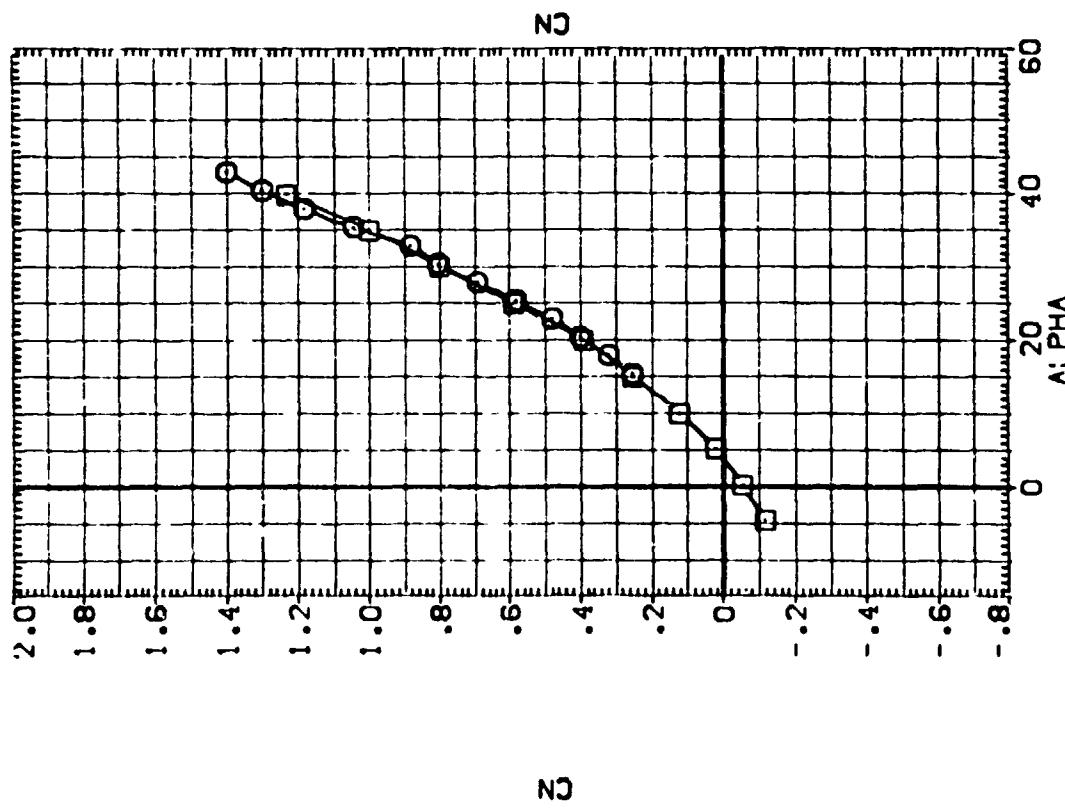
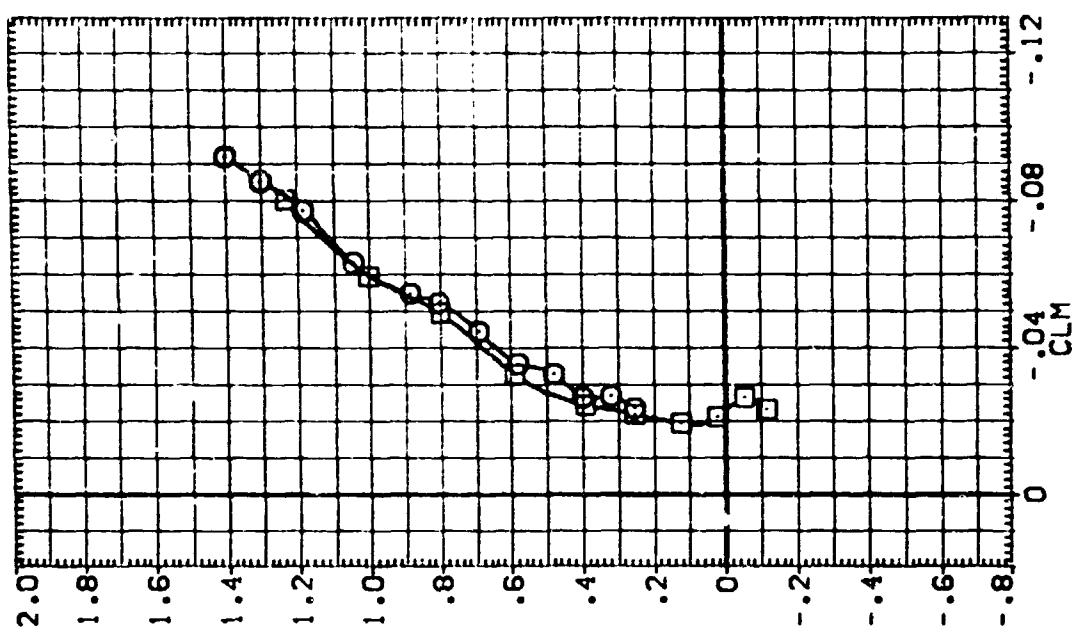


FIGURE 8 EFFECT OF STING SUPPORT ON LONG. CHARACT. (CONTROLS NEUTRAL)
 CA(MACH = 19.80

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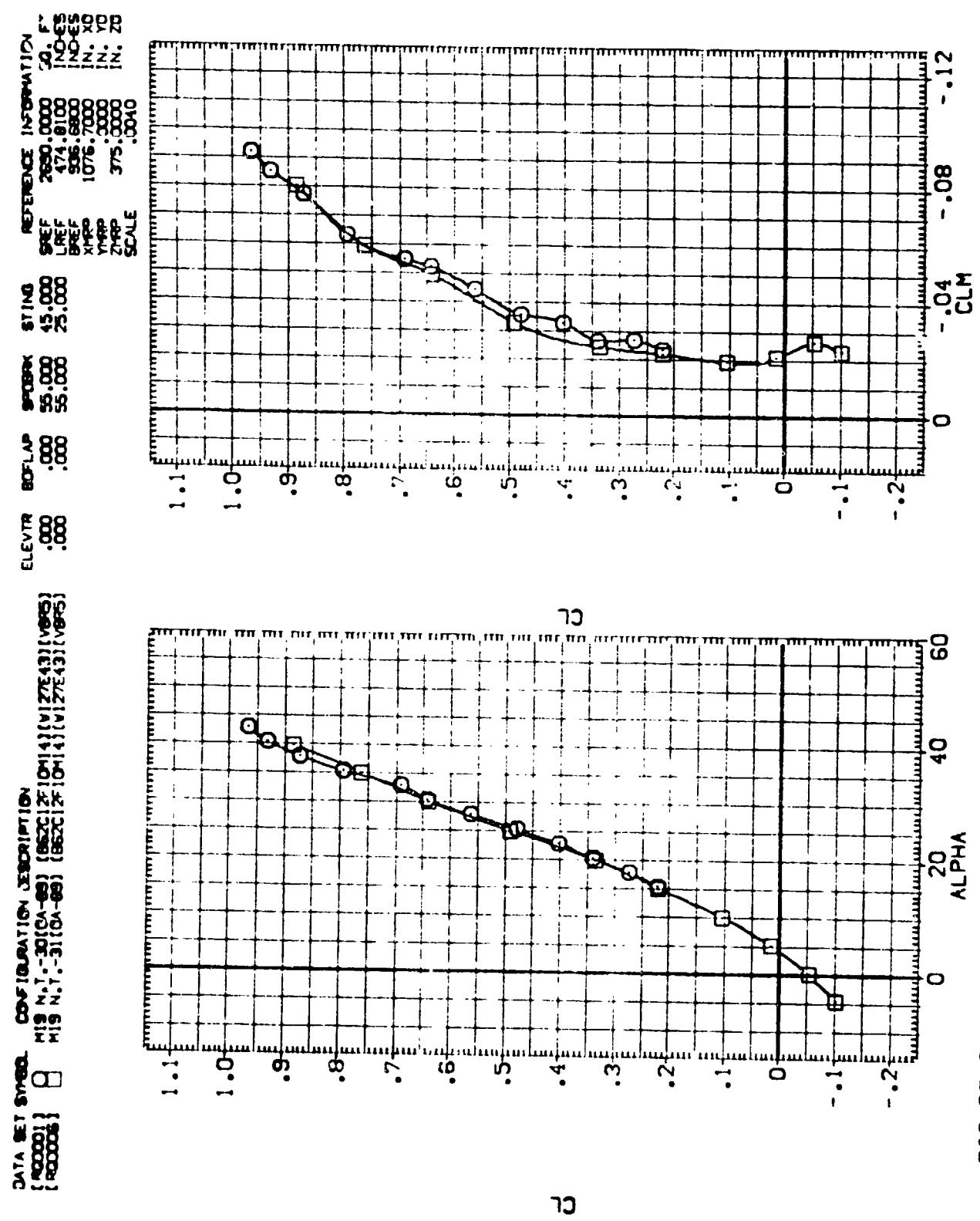


FIGURE 8 EFFECT OF STING SUPPORT ON LONG. CHARACT. (CONTROLS NEUTRAL)
 $(\alpha)_{MACH} = 19.80$

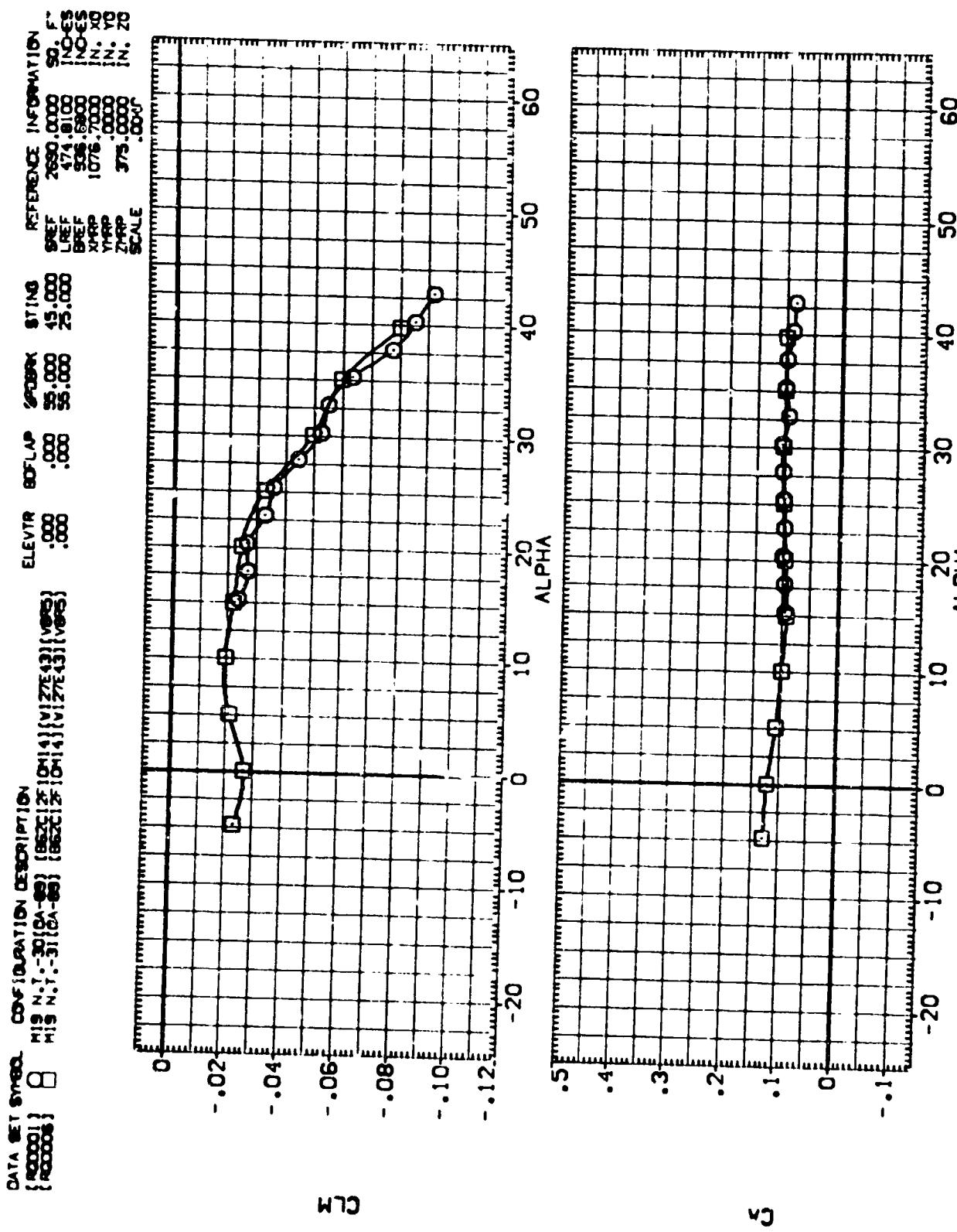


FIGURE 8 EFFECT OF STING SUPPORT ON LONG. CHARACT. (CONTROLS NEUTRAL)
 $(M_{MACH} = 19.8C)$

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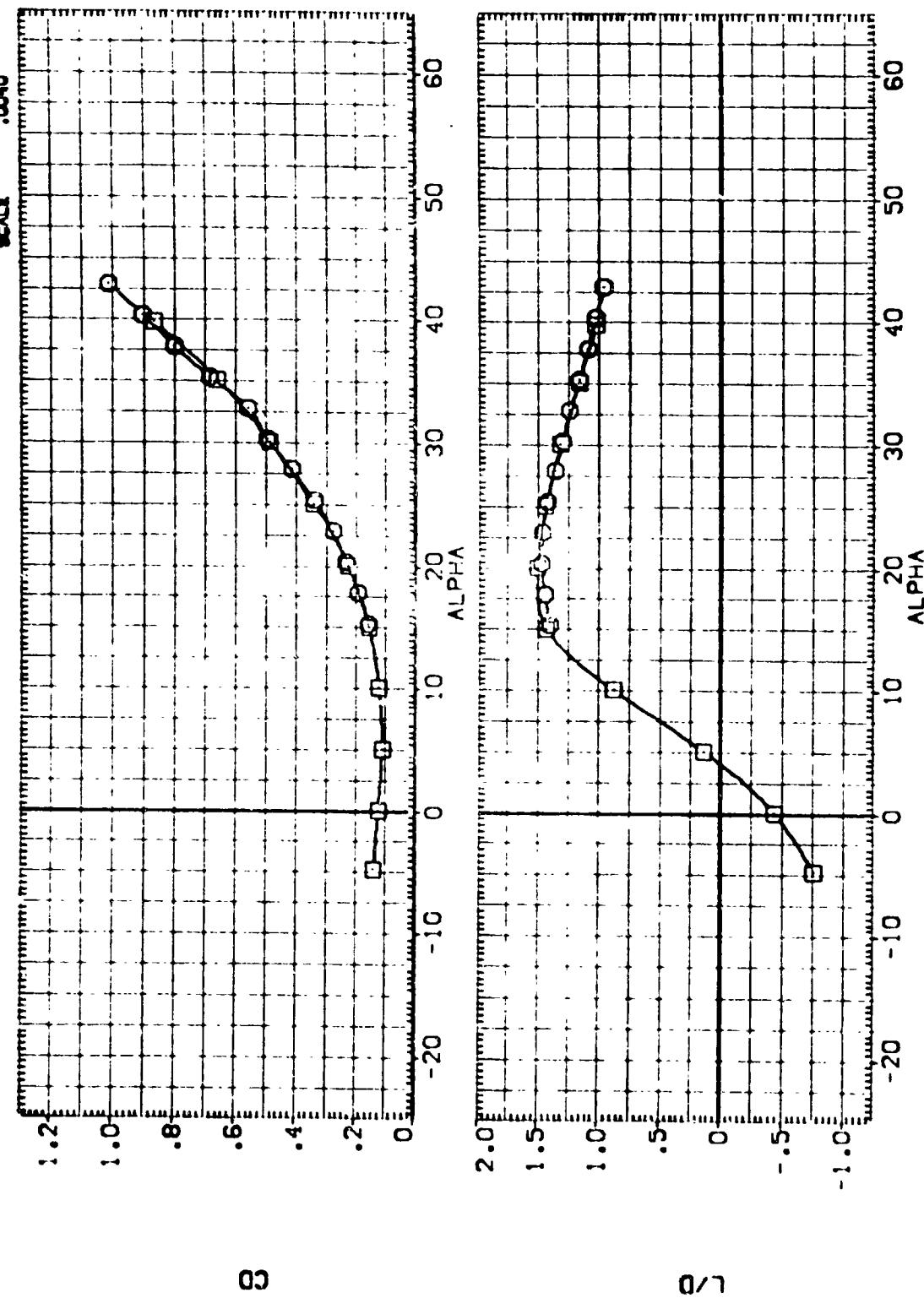


FIGURE 8 EFFECT OF STING SUPPORT ON LONG. CHARACT. (CONTROLS NEUTRAL)

$$[A]_{\text{WACH}} = 19.80$$

DATA SET NAME: CONFIGURATION DESCRIPTION
 [40002] HIGH N.Y.-3(DA-3)
 [40003] HIGH N.Y.-2(DA-2)
 [40004] HIGH N.Y.-1(DA-1)
 [40005] ELEVATOR
 [40006] BDFLAP
 [40007] SPARE
 [40008] STING
 [40009] REFERENCE INFORMATION

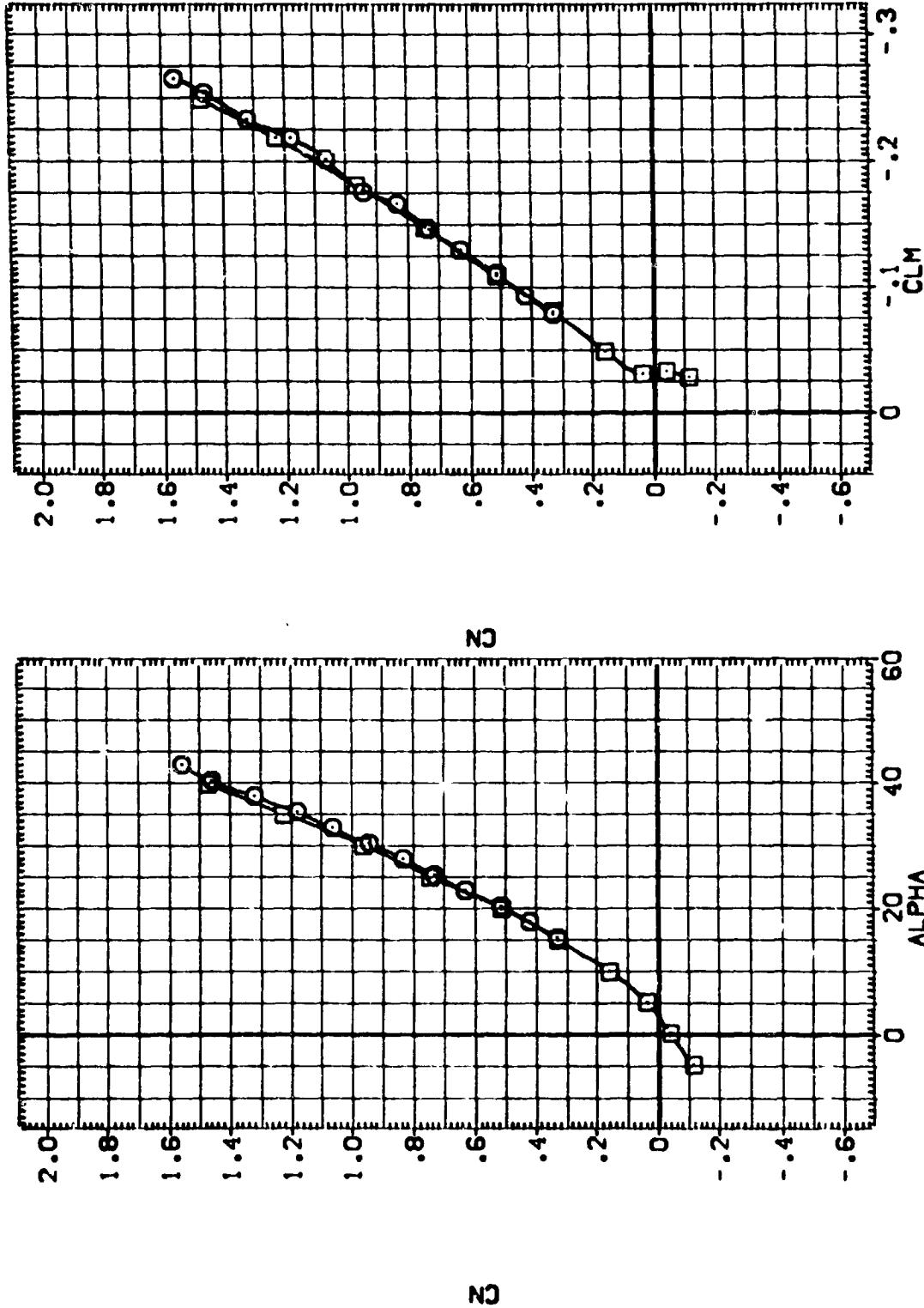


FIGURE 9 EFFECT OF STING SUPPORT ON LONG. CHARACT. (ELEVON= 20, BODY FLAP=16.3)
 $\text{CAIMACH} = 19.80$

DATA SET SYMBOL CONFIGURATION DESCRIPTION
 {
 [] = MIG N.1. -30 [DA-43] [MIG-43] [VZT-43] [VZG-43]
 [] = MIG N.1. -31 [DA-43] [MIG-43] [VZT-43] [VZG-43]

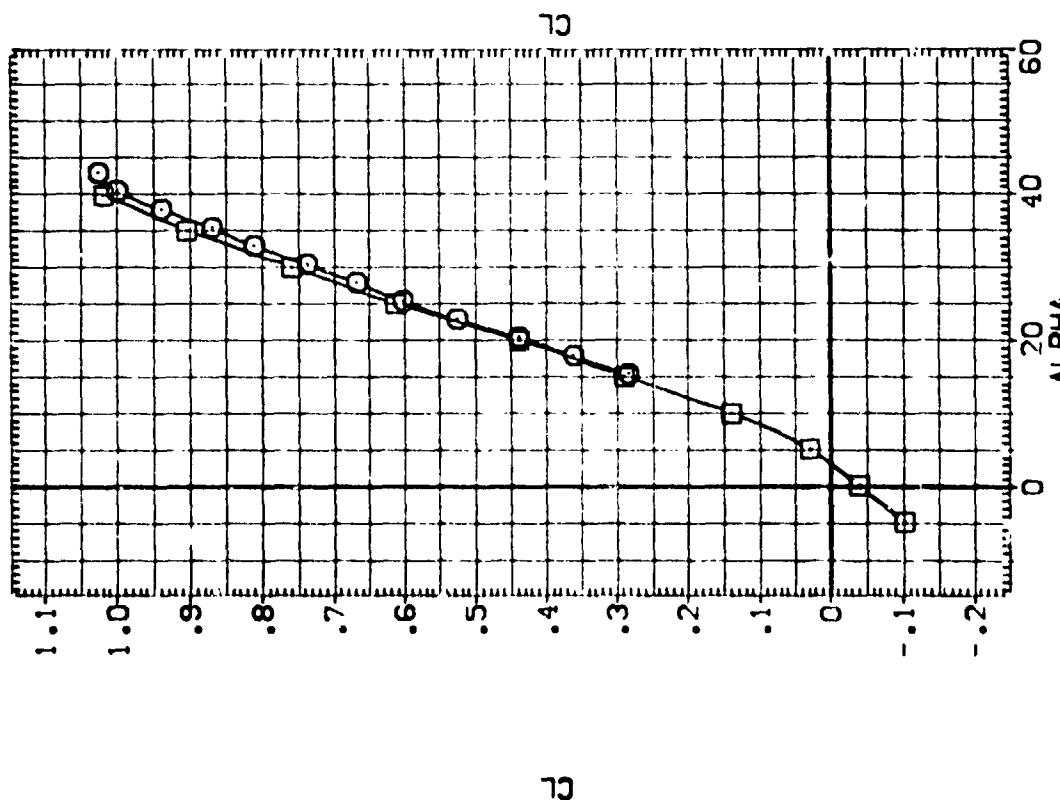
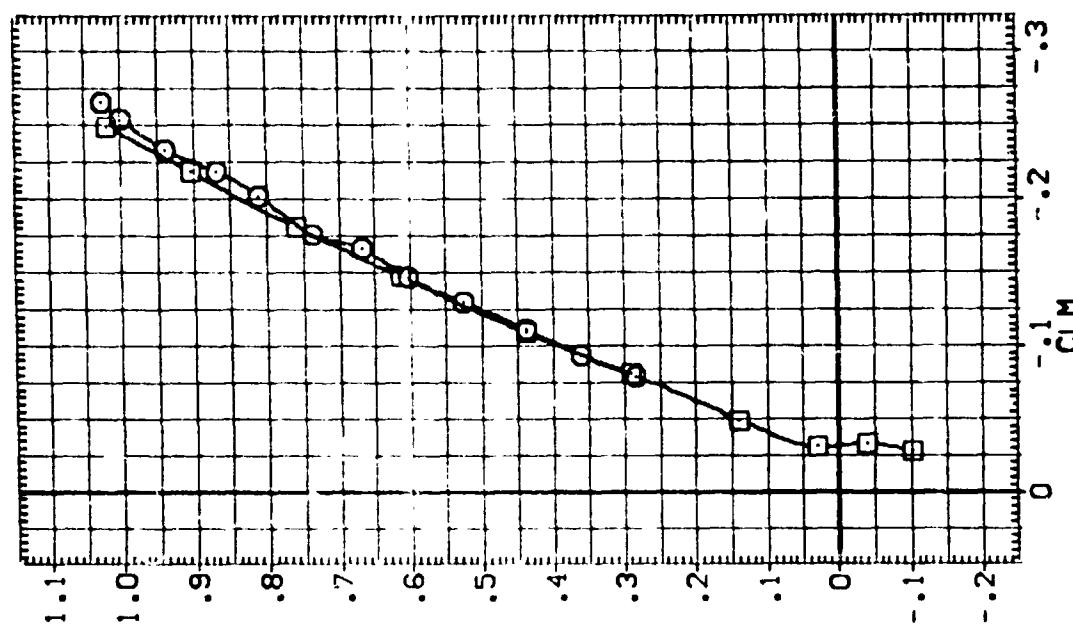


FIGURE 9 EFFECT OF STING SUPPORT ON LONG. CHARACT. (ELEVON= 20, BODY FLAP=16.3)
 (AJMACH = 19.80)

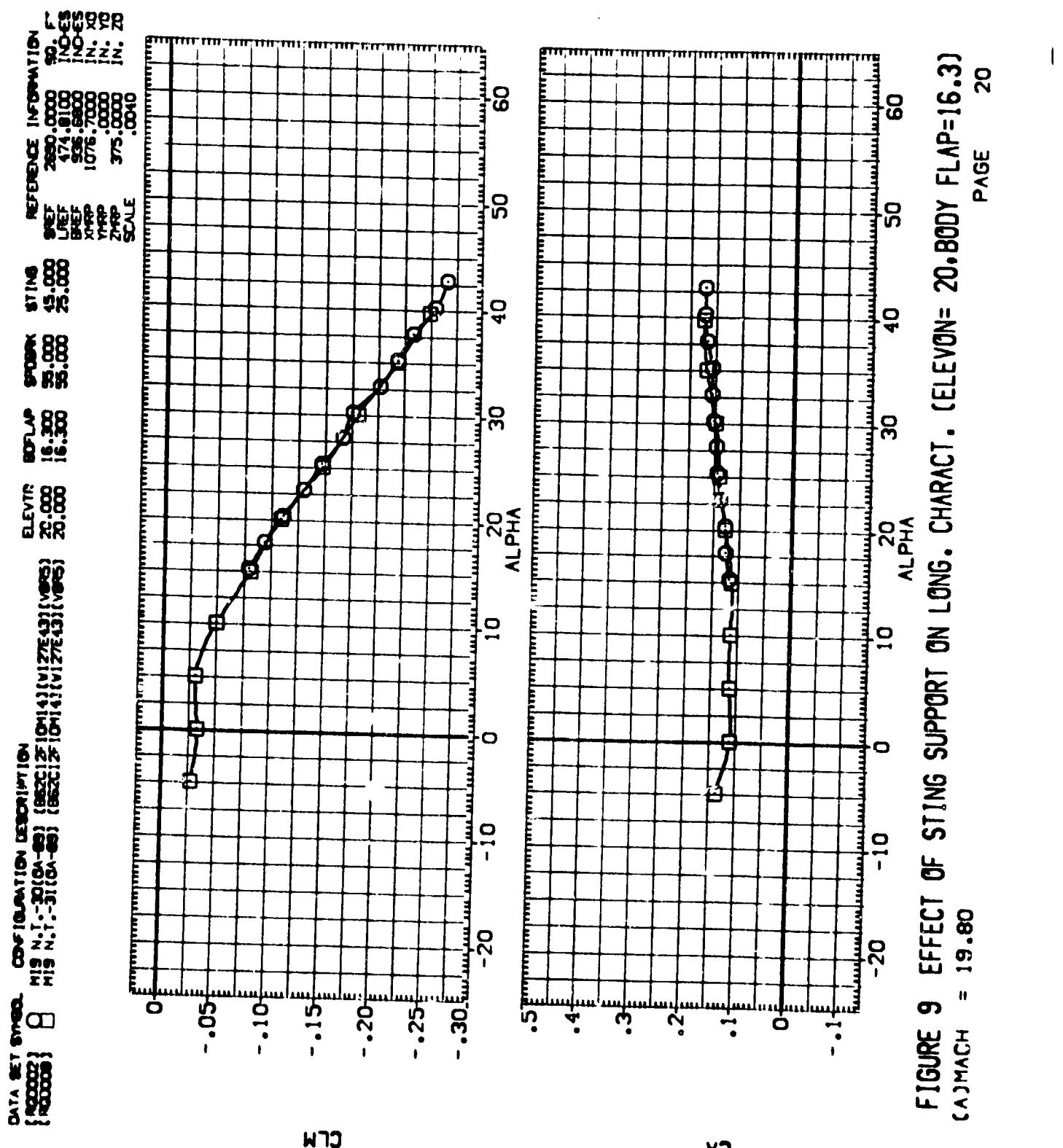


FIGURE 9 EFFECT OF STING SUPPORT ON LONG. CHARACT. (ELEVON= 20, BODY FLAP=16.3)
 $(\alpha)_{MACH} = 19.80$



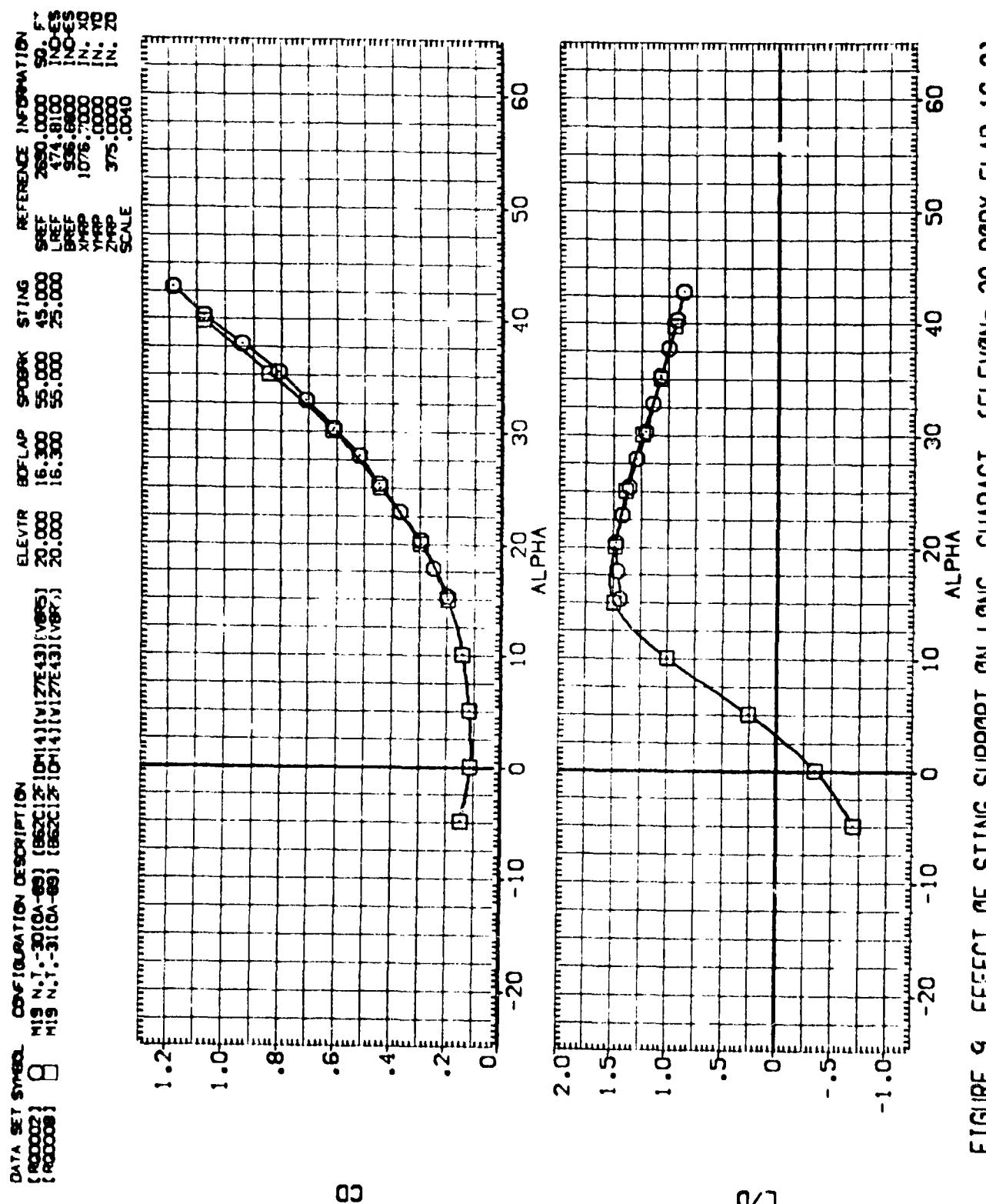


FIGURE 9 EFFECT OF STING SUPPORT ON LONG. CHARACT. (ELEVON= 20, ELEVON= 20, BODY FLAP=16.3)
 C_AMACH = 19.80

APPENDIX
TABULATED SOURCE DATA

Tabulations of plotted data are available on
request from Data Management Services.

DATE 19 MAR 75

ONE SOURCE DATA

PAGE 2

M19 M.7.-30 (A-69) (862C12F10M14) (M27E33) (VERS)

(18 MAR 75)

REFERENCE DATA

SREF =	2000.00000	IN. FT	200P =	1076.0000 IN. NO
LREF =	474.8100	INCHES	TEMP =	.0000 IN. YC
SREF =	936.6077	INCHES	ZREF =	375.0000 IN. ZO
SCALE =	.77143			

RUN NO. 270 0 RNL = .27 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLM	CV	CYN	CL	CD	L/D	XCP/L
19.800	15.323	.32946	.11544	-.07457	.00039	.00030	.00336	.19734	1.41612	.73884
19.820	17.828	.41779	.12485	-.09366	.00193	.000318	.000020	.24677	1.43682	.73290
19.827	20.334	.51255	.12643	-.11069	.00137	.000233	.000009	.29663	1.47215	.72942
19.827	22.842	.62703	.12645	-.13019	.00131	.000235	.000007	.36913	1.42191	.72641
19.827	25.346	.75530	.14276	-.14732	-.00106	.000395	.001341	.44379	1.35966	.72358
19.827	27.832	.89263	.14493	-.16855	-.00140	.000367	.001711	.51711	.29272	.72361
19.827	31.359	.92134	.15256	-.17619	-.00170	.000344	.001619	.60804	1.21075	.71879
19.827	32.865	1.06532	.15563	-.20270	-.00204	.00034	.001336	.70883	1.14524	.72202
19.827	35.371	1.17704	.15716	-.21697	-.00236	.000381	.000951	.80951	1.07325	.71844
19.827	37.887	1.32023	.16666	-.23406	-.002946	.000592	.000972	.94216	.99759	.71524
19.827	40.398	1.49914	.17138	-.25499	-.01036	.000554	.000955	1.07575	.93010	.71431
19.827	42.894	1.55972	.17702	-.26623	-.01094	.000553	.000982	1.16548	.86566	.71286
GRADIENT	.000000	.000000	.000000	.000000	.000000	.000000	.000000	.000000	.000000	.000000

PARAMETRIC DATA

BETA =	.000	ELEVR =	45.000
ATLON =	.000	BDFAP =	16.300
SPARK =	55.000	BALANCE =	1.000
STNG =	45.000		

DATE 10 MAR 74

CASE SOURCE DATA

PAGE 3

M10 N.Y.-D (CA-88) (882C121344) (N22E45W065)

RECORDS (10 MAR 74)

REFERENCE DATA

MACH	ALPHA	CN	CA	CLW	CV	CYN	CL	CD	L/D	XCP/L
16.870	15.321	.21040	.06702	-.03125	.00269	.00152	.17077	.14011	1.22312	.65566
16.871	17.024	.27626	.09011	-.00165	.00168	.00168	.23734	.17096	1.36012	.65570
16.872	20.331	.34316	.09769	-.07191	.00236	.00171	.28766	.21084	1.35530	.65706
16.873	22.837	.42665	.09720	-.07613	.00191	.00125	.33249	.25517	1.35147	.65529
16.875	25.343	.51476	.09356	-.00676	-.01361	.00125	.42113	.32571	1.35352	.65483
16.876	27.849	.59966	.10520	-.00579	-.00517	.00134	.40116	.37316	1.22321	.65356
16.877	30.356	.68116	.10407	-.01131	-.02250	.00128	.49111	.45419	1.22353	.65263
16.878	32.864	.80217	.10756	-.01969	-.02057	.00112	.61341	.52569	1.17177	.65444
16.879	35.372	.91235	.10766	-.01697	-.01392	.00119	.64129	.61352	1.17177	.65282
16.880	37.880	.10150	.10590	-.01474	-.01210	.00117	.65150	.61352	1.17177	.65282
16.877	40.387	1.14110	.09916	-.01414	-.002159	.00117	.81169	.10491	.98775	.65438
16.878	42.894	1.25563	.09246	-.01936	-.02365	.00114	.91293	.92411	.22912	.65560
16.879	44.401	1.37771	.08770	-.01771	-.02721	.00111	.91293	.92411	.22912	.65560

RUN NO. 2A/0 RIVL 3 .27 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLW	CV	CYN	CL	CD	L/D	XCP/L
16.870	15.321	.21040	.06702	-.03125	.00269	.00152	.17077	.14011	1.22312	.65566
16.871	17.024	.27626	.09011	-.00165	.00168	.00168	.23734	.17096	1.36012	.65570
16.872	20.331	.34316	.09769	-.07191	.00236	.00171	.28766	.21084	1.35530	.65706
16.873	22.837	.42665	.09720	-.07613	.00191	.00125	.33249	.25517	1.35147	.65529
16.875	25.343	.51476	.09356	-.00676	-.01361	.00125	.42113	.32571	1.35352	.65483
16.876	27.849	.59966	.10520	-.00579	-.00517	.00134	.40116	.37316	1.22321	.65356
16.877	30.356	.68116	.10407	-.01131	-.02250	.00128	.49111	.45419	1.22353	.65263
16.878	32.864	.80217	.10756	-.01969	-.02057	.00112	.61341	.52569	1.17177	.65444
16.879	35.372	.91235	.10766	-.01697	-.01392	.00119	.64129	.61352	1.17177	.65282
16.880	37.880	.10150	.10590	-.01474	-.01210	.00117	.65150	.61352	1.17177	.65282
16.877	40.387	1.14110	.09916	-.01414	-.002159	.00117	.81169	.10491	.98775	.65438
16.878	42.894	1.25563	.09246	-.01936	-.02365	.00114	.91293	.92411	.22912	.65560
16.879	44.401	1.37771	.08770	-.01771	-.02721	.00111	.91293	.92411	.22912	.65560

GRADIENT

PARAMETRIC DATA

BETA	0.00	ELEV	-35.000
ALIN	0.00	BDFAP	-11.000
SPARK	55.000	BALANCE	1.000
STING	45.000		

DATE 19 MAR 79

CASE SOURCE DATA

PAGE 3

M19 N.T.-31 (OA-89) (862C12 M141 (1985)

(460000) (16 MAR 79)

REFERENCE DATA

SREF = 2697.0000 30. FT XHYP = 1075.0000 IN. XO
 LREF = 474.8173 INCHES YHYP = .0000 IN. YO
 BREF = 936.6871 INCHES ZHYP = 375.0000 IN. ZO
 SCALE = .01463

RUN NO. 32/0 ROLL = .26 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLW	CY	CYN	CL	CD	L/D	XCP/L
19.800	19.320	.07132	.03635	.04271	-.01236	.01574	.05007	.05386	1.01389	.49329
19.800	17.004	.12527	.03652	.04642	-.00127	.00130	.10281	.09021	1.15159	.51361
19.800	20.316	.15224	.03616	.05498	-.00157	.01292	.12332	.09867	1.23731	.51534
19.800	22.810	.19363	.03656	.06629	-.00228	.01291	.15806	.12168	1.30579	.52412
19.800	25.314	.23967	.03595	.06892	-.00370	.01215	.19386	.15158	1.28163	.54332
19.800	27.618	.27980	.03603	.06323	-.00180	.01119	.22114	.16271	1.22813	.54146
19.800	30.321	.31637	.03594	.09199	-.01376	.01529	.24614	.20538	1.19217	.54517
19.800	32.826	.36604	.03668	.11171	-.01952	.01737	.27367	.24791	1.11231	.51171
19.800	35.330	.41349	.03459	.12456	-.02534	.01944	.28356	.216132	.53913	
19.800	37.834	.46299	.03696	.13991	-.01386	.01467	.34374	.14116	1.01569	.52275
19.800	40.341	.53776	.03693	.15904	-.01362	.01823	.57101	.39395	.94619	.56391
19.800	42.846	.59880	.03520	.16449	-.01799	.02471	.40134	.4474	.89677	.54381
19.800	GRADIENT	.07220	.02711	.07111	-.01211	.01471	.07113	.07113	.07113	.07113

M19 N.T.-31 (OA-89) (862C12 M141 (1985)) (VER5)

REFERENCE DATA

SREF = 2697.0000 30. FT MAST = 1376.0000 IN. XO
 LREF = 474.8173 INCHES YHYP = .0000 IN. YO
 BREF = 936.6871 INCHES ZHYP = 375.0000 IN. ZO
 SCALE = .01463

RUN NO. 2/1 ROLL = .21 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLW	CY	CYN	CL	CD	L/D	XCP/L
19.800	-4.756	-.11435	.12633	-.12327	.00615	.00055	-.10340	.13358	-.76436	.57512
19.800	.149	-.15357	.12161	-.12632	.00451	.00052	-.05367	.12356	-.44521	.46783
19.800	.5056	.02544	.10601	-.02193	.01316	.00036	.01401	.1076	.15711	.97891
19.800	10.064	.12330	.09635	-.01931	.00371	-.00026	.10421	.11036	.80732	.73763
19.800	15.074	.25131	.09122	-.12203	-.00352	.00130	.21694	.15144	1.42666	.60226
19.800	21.084	.39227	.09492	-.12446	.071151	.00191	.35582	.22386	1.50113	.67295
19.800	25.198	.58945	.10166	-.03272	.01495	.00116	.49118	.34117	1.33938	.67143
19.800	31.112	.79882	.11115	-.04947	.03124	.00147	.64027	.48625	1.31133	.67279
19.800	35.125	1.17792	.19931	-.05975	.07579	.00212	.76152	.65771	1.15889	.67197
19.800	39.789	1.233161	.19921	-.08126	.101133	.00181	.86442	.66827	1.02163	.67385
19.800	GRADIENT	.01165	-.01119	-.01119	-.01119	.00113	-.01113	-.01113	-.01113	-.01113

(460000) (16 MAR 79)

PARAMETRIC DATA

BETA = .000 ELEVTR = .000
 AILRDN = -.000 DDFLAP = .000
 SPDBRK = .55.000 BALANCE = 1.000
 STING = 25.000

DATE

10 MAR 73

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CLASS SOURCE DATA

M19 N.T.-31 (CH-89) (SEC12F1DM4) (M127E43) (VDR5)

REFERENCE DATA

SREF = 2692.0720 SEC. PT
 LREF = 474.8150 INCHES
 SREF = 936.8670 INCHES
 SCALE = .07400

ROW NO. 370 ROLL = .21 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLM	CV	CYN	CL	CD	L/D	XCP/L
19.870	-4.755	-11106	.12340	-.026682	.002003	.00161	-.10226	.13416	-.74734	.56114
19.870	.057	-.03070	.11445	-.02750	.00146	-.00032	-.000303	.11440	-.44459	.45168
19.870	5.037	.02174	.10873	.02243	.00297	.00121	.00105	.10953	1.02967	
19.870	10.065	.12756	.06976	-.02670	.00161	-.00161	-.001026	.10532	.72737	
19.870	15.075	.27906	.10322	-.04292	.00257	.00257	-.001722	.23675	.17121	.39449
19.870	20.086	.49927	.11252	-.06295	.00186	-.00186	-.001346	.39269	.25341	.49062
19.870	25.100	.86593	.11965	-.08281	.00339	-.00339	-.002953	.36263	.141312	.69582
19.870	30.095	.91596	.13237	-.11596	.00310	-.00310	-.002493	.72611	.57362	.28952
19.870	35.126	1.11023	.12827	-.14766	.00439	-.00439	-.003277	.83426	.74365	.12108
19.870	39.741	1.36296	.13665	-.17364	.00623	-.00623	-.005061	.96861	.96856	.69464
GRADIENT	.01256	-.07228	-.07210	-.07203	-.07244	-.07203	-.071412	.01031	-.02274	

M19 N.T.-31 (CH-89) (SEC12F1DM4) (M127E43) (VDR5)

REFERENCE DATA

SREF = 2692.0720 SEC. PT
 LREF = 474.8150 INCHES
 SREF = 936.8670 INCHES
 SCALE = .07400

ROW NO. 670 ROLL = .20 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CA	CLM	CV	CYN	CL	CD	L/D	XCP/L
19.870	-4.874	-.11425	.13621	-.02735	-.00208	.00164	-.10226	.14549	-.70321	.56191
19.870	.032	-.03936	.11002	-.03310	-.00365	.00156	-.00036	.10948	-.35899	.34070
19.870	5.059	.03664	.11266	-.03092	.00104	.00223	.00275	.11573	.29703	.63360
19.870	10.087	.16184	.11243	-.03621	-.00324	.00133	.00174	.13974	1.02932	.76187
19.870	15.077	.28997	.11132	-.03661	-.00392	.00206	.00264	.19285	1.49363	.76017
19.870	20.087	.51217	.12610	-.10866	.00218	-.00218	.00271	.29434	.14879	.72822
19.870	25.101	.74399	.14223	-.14793	.00393	-.00393	-.00310	.61421	.44260	.13678
19.870	30.113	.95318	.14722	-.18097	.00326	-.00326	-.00253	.75924	.61053	.24357
19.870	35.127	1.22299	.16732	-.21865	.00392	-.00394	-.00314	.84031	1.07597	.71579
19.870	39.842	1.47180	.17274	-.24907	.00479	-.00479	-.00363	.91925	.1.07544	.94775
GRADIENT	.01521	-.07132	-.07117	-.07132	-.07132	-.07132	-.07142	.01274	-.02179	.06988

M19 N.T.-31 (CH-89) (SEC12F1DM4) (M127E43) (VDR5)

PARAMETRIC DATA

BETA = .0000 ELEVTR = 20.000
 ATURON = .0000 BDFLAP = 16.300
 SPDRK = 55.0223 BALANCE = 1.0272
 STINC = 25.0223

M19 N.T.-31 (CH-89) (SEC12F1DM4) (M127E43) (VDR5)

PARAMETRIC DATA

BETA = .0000 ELEVTR = 20.000
 ATURON = .0000 BDFLAP = 16.300
 SPDRK = 55.0223 BALANCE = 1.0272
 STINC = 25.0223

DATE 19 MAR 75

CASE SOURCE DATA

M19 N.T.-31(CA-89) (B62C12F1DM14) (M127E43) (V8R5)

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REFERENCE DATA

SREF = 2690.0000 SQ. FT
 LREF = 474.8175 INCHES YRP = 1076.0000 IN. NO
 BREF = 935.6675 INCHES ZRP = 375.0000 IN. ZO
 SCALE = .0141

RUN NO. 2/0 RFL = .21 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	CN	CLM	CY	CN	CL	CD	L/D	XCP/L
19.877	-4.738	-1.15757	.192131	.020386	.000246	-1.19382	.16572	.88787	.653937
19.877	.048	-0.7419	.122333	-.11395	.02644	-.022269	-.07429	.12047	.61666
19.877	5.055	.00109	.11471	-.000804	.00284	-.00032	-.00002	.11436	.07891
19.877	10.163	1.0344	.10127	-.001524	.00152	-.00021	.00026	.12271	.67664
19.877	15.374	.23872	.101421	-.00249	.00249	-.00033	.00033	.12244	.61648
19.877	21.586	.39732	.102663	-.00361	.00361	-.00049	.00049	.12347	.64616
19.877	25.100	.51750	.10276	-.004691	.004691	-.00052	.00052	.12447	.64356
19.877	31.116	.79397	.11376	-.00673	.00673	-.00054	.00054	.12547	.64721
19.877	35.132	1.02857	.11280	-.00831	.00831	-.00054	.00054	.12647	.64697
19.877	39.793	1.19553	.10815	-.012123	.012123	-.001496	.001496	.12747	.64328
GRADIENT	.01725	-.01665	-.00318	-.00054	-.00054	-.00124	-.00124	.01447	-.01514

M19 N.T.-30(CA-89) (B62C12F1DM14) (M127E43) (V8R5)

REFERENCE DATA

SREF = 2690.0000 SQ. FT
 LREF = 474.8175 INCHES YRP = 1076.0000 IN. NO
 BREF = 935.6675 INCHES ZRP = 375.0000 IN. ZO
 SCALE = .0141

RUN NO. 23/0 RFL = .26 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	Q (PSF)
19.877	15.322	-.00046	.27993	.40 .66197
19.877	17.627	-.00047	.27990	.40 .59217
19.877	20.333	-.00049	.27987	.40 .41921
19.877	22.638	-.00059	.26267	.41 .61636
19.877	25.345	-.00069	.26135	.41 .41570
19.877	27.652	-.00059	.26179	.41 .32164
19.877	30.367	-.00059	.26765	.40 .29976
19.877	32.965	-.00039	.26374	.41 .67649
19.877	35.375	-.00033	.26116	.40 .38595
19.877	37.883	-.00023	.25925	.39 .93507
19.877	40.391	-.00019	.25816	.39 .92107
19.877	42.899	-.00032	.26169	.40 .31331
GRADIENT	.02471	.02471	.02471	.02471

(AGD711) (10 MAR 75)

PARAMETRIC DATA

BETA = .000
 ATLRCH = .000
 SPDRK = .55 .000
 STING = 49.071

(AGD711) (10 MAR 75)

PARAMETRIC DATA

BETA = .000
 ATLRCH = .000
 SPDRK = .55 .000
 BALANCE = 1.000

DATE 19 MAR 73

CASE SOURCE DATA

MIS M.T.-E (CH-69) (B8C12F10M14) (M27E43) (VERS)

REFERENCE DATA

SREF	2093.0775	36. FT	XREF	1076.7000	14. NO
LREF	4/4.0121	INCHES	YREF	.0000	14. TO
BREF	935.6022	INCHES	ZREF	375.0000	14. ZO
SCALE	.0041				

RUN NO. 26V0 RNL = .27 GRADIENT INTERVAL = -.00/ 1.00

MACH	ALPHA	BETA	RN	Q (PSF)
19.800	15.323	-.02116	.26669	.00.31331
19.800	17.026	-.02206	.26840	.00.24267
19.800	20.334	-.02291	.26802	.00.18556
19.800	22.141	-.02297	.26792	.00.16004
19.800	25.346	-.02292	.26724	.00.06634
19.800	27.852	-.022076	.27015	.00.20217
19.800	30.159	-.02202	.26988	.00.45036
19.800	32.065	-.022051	.26979	.00.29470
19.800	35.371	-.022144	.26782	.00.13351
19.800	37.987	-.022335	.26. -1	.00.22261
19.800	40.386	-.02226	.26869	.00.28326
19.800	42.894	-.022222	.26879	.00.29470
	GRADIENT	GRADIENT	GRADIENT	

PAGE 1

(A00721) (18 MAR 73)

PARAMETRIC DATA

BETA	= .000	Q.EVNTA = 20.000
ALPHON	= .000	BOP, LAP = 16.320
SPARK	= 33.073	BALANCE = 1.000
STING	= 45.000	

PAGE 2

DATE 10 MAR 75

CASE SOURCE DATA

M19 M.F.-33 (CA-60) (862C12F10M14) (M127E13) (V883)

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(10000) (10 MAR 75)

REFERENCE DATA

SREF =	2697.0000 IN.	XREF =	1076.0000 IN.	ZREF =	1076.0000 IN.
LREF =	474.8120 INCHES	YREF =	.073 IN.	Y0 =	.073 IN.
BREF =	936.6000 INCHES	ZREF =	375.0000 IN.	Z0 =	20
SCALE =	.7741				

RUN NO. 2870 RNU = .27 GRADIENT INTERVAL = -.500/ .500

MACH	ALPHA	BETA	RN	Q (PSF)
19.870	15.321	-.02233	.26792	40.16034
19.870	17.826	-.02233	.26792	40.16034
19.870	20.331	-.02233	.26621	40.21162
19.870	22.837	-.02232	.26641	40.24367
19.870	25.343	-.02234	.26995	40.47311
19.870	27.849	-.02233	.27115	40.53217
19.870	30.356	-.02234	.27375	40.48764
19.870	32.864	-.02232	.27375	40.49764
19.870	35.372	-.02233	.26986	40.45556
19.870	37.879	-.02232	.26966	40.42253
19.870	40.387	-.02233	.26995	40.47311
19.870	42.894	-.02236	.26995	40.47311
		.02231	.26995	

GRADIENT

GRADIENT INTERVAL = -.500/ .500

PARAMETRIC DATA

BETA =	.000	ELEVTR =	-.55.000
AIRCON =	.000	BLDFLAP =	-11.000
SPDRK =	.55.000	BALANCE =	1.000
STRNG =	45.000		

DATE 10 MAR 75

SOURCE DATA

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M19 N.7.-37 (OA-89) (B62C12F10M14) (WRS5)

(A00004) (10 MAR 75)

REFERENCE DATA

SREF	2691.7700 50. FT	ZDRP	1076.7000 IN. 10
LREF	474.6100 INCHES	YDRP	.0000 IN. 10
BREF	936.6875 INCHES	ZDRP	375.0000 IN. 20
SCALE	.17461		

RUN NO. 3510 RNL = .27 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	Q (P95)
19.800	15.320	-.000192	.26962	40.70355
19.800	17.825	-.000223	.26924	40.61636
19.800	21.331	-.000112	.26956	40.51669
19.800	22.835	-.000299	.26926	40.47311
19.800	25.340	.000020	.26731	40.32784
19.800	27.847	.000221	.26606	40.13896
19.800	30.355	.000195	.26491	39.96465
19.800	32.861	.000120	.26385	40.56726
19.800	35.369	.000054	.26016	40.45856
19.800	37.879	.000099	.26993	40.26973
19.800	40.384	.000237	.27153	40.96704
19.800	42.892	.000335	.27330	40.77619
	GRADIENT	.000000	.000000	

PARAMETRIC DATA

BETA	0	ELEVAT	.000
AILRON	10.00	EDFLAP	-11.00
SPOILER	55.00	BALANCE	1.000
STING	45.00		

DATE 19 MAR 75

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CASE SOURCE DATA

M19 N.Y.-31 (CA-89)

(B62C12) (M14) (V8R5)

REFERENCE DATA

SREF = 2695.0000 30. FT XREF = 1076.0000 IN. NO
 LREF = 474.0100 INCHES YREF = .0000 IN. TO
 BREF = 936.0000 INCHES ZREF = 375.0000 IN. ZO
 SCALE = .07461

RUN NO. 32/0 RAVL = .20 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	Q (PSF)
19.800	15.300	-.00020	.27070	40.48764
19.800	17.604	-.000235	.27040	40.44406
19.800	20.306	-.000237	.26190	40.95251
19.800	22.810	-.000229	.26160	40.93799
19.800	25.314	-.000221	.26160	40.93799
19.800	27.618	-.000212	.26190	40.95251
19.800	30.1321	-.000203	.27030	40.57480
19.800	32.026	-.00010	.27690	40.51669
19.800	35.323	.00015	.27660	40.47311
19.800	37.036	-.000024	.27660	40.47311
19.800	40.341	-.000036	.27630	40.42953
19.800	42.646	-.000092	.27660	40.47311
19.800	GRADIENT	.000200	.000200	.000200

M19 N.Y.-31 (CA-89) (B62C12F1DM14) (M12/E43) (V8R5)

(AQD005) (19 MAR 75)

REFERENCE DATA

SREF = 2695.0000 30. FT XREF = 1076.0000 IN. NO
 LREF = 474.0100 INCHES YREF = .0000 IN. TO
 BREF = 936.0000 INCHES ZREF = 375.0000 IN. ZO
 SCALE = .07461

RUN NO. 0/0 RAVL = .21 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	Q (PSF)
19.800	-4.756	-.00029	.20851	40.63159
19.800	.049	-.000166	.21020	40.92147
19.800	5.056	-.000154	.20660	40.31265
19.800	10.364	-.000037	.20673	40.28566
19.800	15.074	-.000223	.210959	40.70413
19.800	23.084	-.000337	.20800	40.70413
19.800	25.098	-.000149	.21095	40.70513
19.800	30.112	-.000355	.21084	40.61766
19.800	35.125	-.000154	.20835	40.60256
19.800	39.789	-.000217	.210821	40.57357
19.800	GRADIENT	.000205	.000205	.000204

(AQD006) (19 MAR 75)

PARAMETRIC DATA

BETA = .0000 SPARK = .0000
 BALANCE = 1.0000 STING = .0000

BETA = .0000 ELEVTR = .0000
 AILRON = .0000 BOFLAP = .0000
 SPARK = .0000 BALANCE = 1.0000
 STING = 25.0000

DATE 10 MAR 75

CRSS SOURCE DATA

M19 N.T.-31 (OA-89) (B62C12F10M14) (M12TE43) (VER5)

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(ADD071) (10 MAR 75)

REFERENCE DATA

SREF	2600.00000	SL. PT	ZMP	0	1076.7000 IN. NO
LREF	474.8103 INCHES	YMP	=	.0000 IN. YO	
SREF	936.6800 INCHES	ZMP	=	375.0000 IN. ZO	
SCALE	.0240				

RUN NO. 3/0 RNL = .21 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	G(PSF)
19.870	-4.755	-.007042	.23036	40.80256
19.870	.050	-.007033	.23057	40.34456
19.870	5.057	-.007036	.23777	40.46660
19.870	10.065	-.007010	.20782	40.45761
19.870	15.075	-.007020	.20747	40.42861
19.870	20.086	-.007017	.20702	40.34164
19.870	25.100	-.007029	.20702	40.34164
19.870	30.095	-.007037	.20717	40.37063
19.870	35.126	-.007032	.20926	40.77651
19.870	39.741	-.007050	.20911	40.74752
GRADIENT	.007002	-.007006	-.01207	

M19 N.T.-31 (OA-89) (B62C12F10M14) (M12TE43) (VER5)

REFERENCE DATA

SREF	2600.00000	SL. PT	ZMP	0	1076.7000 IN. NO
LREF	474.8103 INCHES	YMP	=	.0000 IN. YO	
SREF	936.6800 INCHES	ZMP	=	375.0000 IN. ZO	
SCALE	.0240				

RUN NO. 0/0 RNL = .20 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	RN	G(PSF)
19.870	-4.874	-.007026	.20512	40.19668
19.870	.932	-.007003	.20506	40.34164
19.870	5.059	-.007017	.20490	40.15319
19.870	10.067	-.007011	.20430	40.03723
19.870	15.077	-.007011	.20408	39.99374
19.870	20.097	-.007017	.20393	39.96475
19.870	25.101	-.007034	.20386	39.95225
19.870	30.113	-.007035	.20364	39.90267
19.870	35.127	-.007037	.20371	39.92126
19.870	39.842	-.007050	.20364	39.95677
GRADIENT	.007015	-.007015	.02943	

PARAMETRIC DATA

BETA	= .0000
AIRCON	= .0000
SPDRK	= 55.0000
STING	= 25.000

PARAMETRIC DATA

BETA	= .0000
ELEVTR	= 20.000
SDFLAP	= 16.000
BALANCE	= 1.000

PARAMETRIC DATA

BETA	= .0000
AIRCON	= .0000
SPDRK	= 55.0000
STING	= 25.000

PARAMETRIC DATA

BETA	= .0000
ELEVTR	= 20.000
SDFLAP	= 16.000
BALANCE	= 1.000

DATE 19 MAR /5

CASE SOURCE DATA

M19 M.T.-31 (CH-89) (B2C12P10M1) (M127E43) (W01)

REFERENCE DATA

SURF	=	2000.0000 IN.	FT	TEMP	=	1976.0000 IN.	IN	Q
LREF	=	474.6103 INCHES		TEMP	=	.00223 IN.	YD	
BREF	=	936.6000 INCHES		ZMP	=	375.0000 IN.	20	
SCALE	=	.0046						

RUN NO. 2/0 ANPL = .21 GRADIENT INTERVAL = -5.00/ 5.00

	MACH	ALPHA	BETA	MN	BN(PGF)
19.870	-4.756	-.00152	.20747	40.42861	
19.870	.048	-.00049	.20695	40.32714	
19.870	2.755	-.00021	.20695	40.32714	
19.870	10.163	-.00021	.20695	40.32714	
19.870	15.074	-.00027	.20713	40.35613	
19.870	20.086	-.00024	.20777	40.46697	
19.870	25.100	-.00041	.20851	40.63155	
19.870	30.116	-.00034	.20926	40.77651	
19.870	35.132	-.00043	.21037	41.93597	
19.870	39.793	-.00047	.21916	40.76292	
GRADIENT		-.00021	-.02111		

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(A00279) (19 MAR /5)

PARAMETRIC DATA

BETA	=	.0000	BLVTR	=	-40.000
ATLON	=	.0000	BLFLAP	=	-11.700
SPORH	=	55.000	BALANCE	=	1.000
STING	=	25.000			